1980 CRC FUEL RATING PROGRAM: ROAD OCTANE PERFORMANCE IN 1980 MODEL CARS

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1980 CRC FUEL RATING PROGRAM: ROAD OCTANE PERFORMANCE IN 1980 MODEL CARS

(CRC Project No. CM-124-80)

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Prepared by the

1980 Analysis Panel

of the

CRC - Road Test Group

July 1981

Light-Duty Vehicle Fuel, Lubricant, and Equipment Research Committee of the

Coordinating Research Council, Inc.

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I. INTRODUCTION

Road octane rating programs have been conducted periodically since 1963 by the Coordinating Research Council (CRC) Light-Duty Vehicle Road Test Group to investigate relationships between gasoline variables and road octane numbers. Leaded gasolines were tested during the 1963 - 1969 period; unleaded gasolines were tested in the 1971, 1973, 1975, and 1978 programs. This is the eleventh program in the series and includes gasoline blends containing ethanol (gasohol) in addition to normal gasoline variables.

Full-Throttle Modified Uniontown Road Octane Numbers (Road ON) were obtained by twelve participating laboratories in thirty-seven cars that represent twenty-four different 1980 makes and models, one 1979 model, and one 1981 model. Part-throttle Road ON ratings were obtained by four participating laboratories in twelve cars representing nine different 1980 makes and models.

II. SUMMARY

The data were analyzed using multiple linear regression and analysis of variance techniques. Analyses were made on all-car average data, as well as data from individual cars and from several subgroups. On an all-car basis, full-throttle Road ON's were found to be well predicted by the following equation containing only Research octane number (RON) and Motor octane number (MON):

Road ON = 26.275 + 0.286 (RON) + 0.450 (MON)

The equation fit was improved considerably (lower standard deviation), however, by first adding a $(RON)^2$ term, then adding a term for heavy aromatics content:

Road ON = $-163.216 + 4.294(RON) - 0.021(RON)^2 + 0.432(MON) - 0.012 (Heavy Aromatics)$

This equation indicates that the effect of RON on Road ON decreases with increasing RON level, and that heavy aromatics have an adverse effect on Road ON which is independent of its direct effects on RON and MON.

>The all-car data did not show a significant ethanol-content effect, but eight of the thirty-seven cars did show significant effects.

Analysis of variance showed that fuels had the largest effect on full-throttle Road ON. Cars had smaller, but highly significant, effects. The effects of fuels on Road ON varied among the cars.

The part-throttle ratings were also well predicted with an equation containing only RON and MON:

Road ON = 32.008 + 0.091 (RON) + 0.553 (MON)

Equation fit was improved by adding a heavy aromatics term, but ethanol did not have a significant effect on the average part-throttle Road ON:

Road ON = 31.823 + 0.089(RON) + 0.559(MON) - 0.009 (Heavy Aromatics)

Only one car showed a significant effect of ethanol at part-throttle.

Analysis of variance showed that cars had a larger effect than fuels on the part-throttle ratings. The reverse was true for the full-throttle ratings. The effects of fuels did not vary among the cars, as they did with the full-throttle ratings.

III. DESCRIPTION OF PROGRAM

Appendix A lists the participating laboratories in the 1980 program and the membership of the Analysis Panel. The program is presented in Appendix B. Fuel properties, test car descriptions, the road rating procedure, and a brief outline of data analyses employed are summarized in the following paragraphs.

A. Test Fuels

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The twenty unleaded test fuels used in the program were designed to estimate the effects of RON, MON, heavy aromatics content (Cg and heavier, by volume), and ethanol content (by volume) on Road ON performance. A computer optimization program was used to design the fuel set. The optimization provided for the evaluation of $(RON)^2$ and $(MON)^2$ effects, in addition to linear effects for the four variables. There were three levels of RON, five levels of MON, and two levels each of heavy aromatics and ethanol. (R+M)/2 ranged from 86.4 to 93.4 ON, and sensitivity ranged from 5.6 to 12.8 ON.

Laboratory inspection data for the twenty fuels submitted by the participants were screened for outliers. All outliers were rejected, and the remaining values were averaged. Targeted and actual values for the four variables are compared in Table I. Many of the RON and MON values were more than one octane number off target, and some of the heavy aromatics and ethanol values were not within limits. The test fuel set was still found, however, to be capable of very good evaluation of the effects of the four parameters. This is indicated by the low

correlations among the four design parameters, as shown in Table II. The RON/MON correlation is not as low as the others, but it is approximately the same as in the 1978 program (0.784 versus 0.779), and it is difficult to design a set of fuels with a RON/MON correlation much less than 0.8. Low correlation values are necessary for accurate determination of the effects of the four parameters.

Volatility and total aromatics data are shown for the test fuels in Table III. Only six fuels met the RVP requirement of 8-10 lbs. The other fuels had RVP's below 8 lb. All fuels met the distillation and total aromatics specifications. The test fuel specifications are shown in Appendix B.

B. <u>Test Cars</u>

Thirty-seven cars representing twenty-four different 1980 models, one 1979 model, and one 1981 model were used in the program. Only two cars, T 218M and PL 217M, were equipped with manual gear-shift transmission, and the remaining cars had automatic transmissions. The test car models and their engine characteristics are shown in Table IV. The car-laboratory testing array for both full- and part-throttle Road ON is shown in Appendix C. The odometer readings ranged from 7,115 to 42,134; and the mean was 15,741 miles. The odometer reading is shown in Appendix H for each test car, along with other test details.

C. Road Rating Technique

Fuel ratings were obtained by the Modified Uniontown Technique under both full- and part-throttle conditions. Full-throttle primary reference fuel curves were used to establish the Road ON under full-throttle conditions. Part-throttle primary reference fuel curves were used to establish the Road ON at part-throttle. Thirty-seven cars were tested at Suil-throttle, and twelve of these cars were also tested at part-throttle. All ratings were conducted on chassis dynamometers. The CRC Modified Uniontown rating technique is described in Appendix D.

D. Data Analysis

Analyses were conducted on both full-throttle and part-throttle data. Other subgroups of data were analyzed, including all-car averages, all-automatic-transmission-car averages, all-U.S.-car averages, all-imported-car averages, model averages, and individual cars. Linear and second-order equations were developed using RON, MON, (RON)2, (MON)2, heavy aromatics, and ethanol content as variables. Analysis of variance (ANOVA) techniques were used to evaluate individual contributions of cars, fuels, car-fuel interactions, and test error to the variability of the road test ratings.

IV. DISCUSSION OF RESULTS

A. Test Results

Average full-throttle and part-throttle Road ON ratings for the twenty test fuels are listed in Tables Va and Vb, together with the standard deviations and the minimum and maximum ratings for each fuel. Because of difficulties with three of the ethanol-containing fuels, twenty-one missing data points at full-throttle and twelve at part-throttle were estimated. In addition, one data point on Fuel 15, a non-ethanol fuel, was estimated. Road ON estimates were made by developing a prediction equation for each car that did not test all fuels, and then calculating the missing Road ON. The use of these estimated ratings completed the data set in Table Va which covers all thirty-seven cars at full-throttle and twelve cars at part-throttle. Table Vb gives the average values when only the vehicles in which all fuels were rated are included. The average full-throttle ratings varied from 89.3 to 94.2 ON and 88.9 to 93.9 ON among the twenty test fuels for the 37-car and 26-car data sets, respectively. Individual fuel ratings varied as much as 7.3 ON (Fuel 7) among the thirty-seven cars, and 5.3 ON (Fuel 17) among the twenty-six cars.

The twelve-car average part-throttle ratings were 3.8 ON lower than the thirty-seven full-throttle ratings. The eight-car part-throttle ratings were 3.5 ON lower than the twenty-six full-throttle ratings on the average. Individual fuel ratings varied as much as 8.7 ON (Fuel 20) among the twelve cars, and 6.6 ON (Fuel 16) among the eight cars.

Three import car models (E 215, T 218M, and T 222), three models having the same engine (one M V250 and two 0 V250's), and four Model PC 137's were tested. Average full-throttle ratings for these selections are listed in Appendix E, Table E-1.

Average full-throttle ratings for each of the thirty-seven cars are listed in Table E-2. Average part-throttle ratings for each of the twelve cars are listed in Table E-3. Individual experimental observations are tabulated in Appendix H.

B. Full-Throttle Data Analysis

1. Multiple Regression Analysis

A total of twenty-nine equation models were developed, as shown in Table VI. Six of these equations were used for only those indiviual car analyses where RON or MON was not a significant variable. Results of the aralyses are shown in Appendix F for both full-throttle and part-throttle ratings. Full-throttle results are presented in Tables F-1 through F-9. Equation models 1-16 are shown in Table F-1 using the all-car average data. Equation models 1-6 are shown in Tables F-2 through F-8 for all cases: car model averages (three or more of the same model), all-car averages, all-car averages testing all fuels, all-U.S.-car averages, all-automatic-transmission-car averages. all-imported-car averages, and individual cars. Equation models 3, 8, and

10 were used for a 37-car individual data analysis and are shown in Table F-9. For the individual car cases, additional equations are shown where all terms are significant.

a. All-Car Average Data

The all-car average results show that Road octane ratings were predicted best by Equations 3, 7, 8, and 10. As shown below, these equations include only the RON, MON, (RON)², and heavy aromatics terms. The inclusion of the ethanol term as well as other quadratic terms did not improve prediction accuracy, and their coefficients were not statistically significant at the 95% confidence level.

Full-Throttle Regression Equations For 37-Car Road ON Averages

Equation Model	Constant b _o	RON b ₁	MON b ₂	Heavy Aromatics ^b 3	Ethanol ^b 4	(R+M)/2 b ₅	(RON) ²	Std. Dev.	R ²
3	26.275	0.286	0.450		_			0.276	0.977
4	26.005	0.284	0.457	<u>-0.009</u>				0.269	0.979
5	26.599	0.300	0.430		0.015			0.275	0.979
6	26.616	0.295	0.437	-0.009	0.014			0.269	0.981
7	29.700					0.690		0.296	0.972
8	-143.663	3.997	0.425				-0.020	0.209	0.988
10	-163.216	4.294	0.432	-0.012			-0.021	0.178	0.991
10*	-174.765	4.613	0.420	-0.011			-0.023	0.169	0.992

NOTE: Underlined values are not significant at the 95% confidence level.

^{* 26-}car average equation. Eleven cars that did not rate all design fuels were eliminated.

The inclusion of the $(RON)^2$ and heavy aromatics terms (Equation 10), along with RON and MON, substantially improved prediction accuracy over Equation 3; the standard deviation was reduced from 0.276 to 0.178, and the square of the coefficient of correlation (R^2) was increased from 0.977 to 0.991. It is interesting to compare Equation 4 with Equation 10 and to note that the heavy aromatics term was not significant (Equation 4), unless the $(RON)^2$ term was used (Equation 10).

The last equation shown is based on those twenty-six cars that rated all twenty fuels, and is shown for comparison.

Prediction of the 37-car average full-throttle Road ON using Equations 3, 8, and 10 are shown in Figures 1, 2, and 3, respectively. The improvement in prediction accuracy is illustrated.

The 37-car average equation model (Equation 8), in terms of RON, MON, and (RON)², demonstrates the effect of fuel octane level on the relative contribution of RON and MON to Road ON quality. For premium unleaded type fuels, for example, a change in RON will have little effect on actual Road octane quality, whereas the opposite is true for regular unleaded type fuels. This effect is shown in Table VII for the linearized second-order model.

b. Individual Car Data

The observed individual Road ON ratings for the thirty-seven cars versus predicted Road ON ratings for all twenty fuels is shown in the scatter diagram on Figure 4. Regressing the individual ratings gave results similar to the all-car average data; the coefficients were essentially the same. The large standard deviations shown in Table F-9 are due to variations in ratings among the thirty-seven cars. These variations are not present when all-car average data are used.

The coefficient for the ethanol term was significant in eight of the thirty-seven cars (22%) tested. All but two of these coefficients were positive, indicating a possible Road octane bonus for these cars. This is in contrast to the all-car average results which showed that the ethanol term was insignificant in combination with any other terms.

Road ON averages and regression results varied considerably among the thirty-seven cars. The following table shows these variations in the twenty-fuel average full-throttle Road ON's (standard deviations and ranges), as well as the means; the standard deviations; and the ranges for the constant, RON, and MON coefficients for Equation 3 regression parameters.

Variation of Full-Throttle Road ON Regression Results Among Cars

	Mean	Standard Deviation	Min.	Max.
Full-Throttle Road ON (37 Cars)	91.903	1.051	89.725	94.845
Full-Throttle Road ON (Equation 3) Constant, b	25.885	13.194	-7.256	44.110
RON Coefficient, b ₁	0.285	0.119	0.036	0.588
MON Coefficient, b ₂	0.456	0.142	0.146	0.729

The RON coefficients varied from near zero to approximately 0.6, the MON coefficients from approximately 0.1 to 0.7, and the constant from -7 to 44.

2. Analysis of Variance (ANOVA)

The full-throttle data were subjected to ANOVA techniques to evaluate the overall contributions of fuel effect, car effect, car-fuel interaction, and test error to the variability in the observed Road octane ratings.

The fuel effect, a measure of the variation caused by fuel composition, was highly significant and caused most of the variability -- about 65%.

The car effect, a measure of the difference in ratings between cars, was highly significant and caused about 20% of the variability observed. The car effect is confounded with the laboratory effect, though; hence, the two effects cannot be separately determined.

The car-fuel interaction, the variation resulting from the differences in response of individual cars to individual fuels, was significant and accounted for about 7% of the variability.

Error, a measure of the variability of replicate ratings, represented about 8% of the total variability.

Standard deviations of the effects are summarized below for all cars (except E 215), and for two models for which three or more of the same model were tested. A more detailed tabulation of the ANOVA results is given in Appendix G.

Analysis of Variance Summary for All Cars and for Two Car Hodels

	No. of	Estimated Standard Deviation (s-Values)						
Car Model	Cars	Cars	Fuels	Fuel x Car	Error			
All Cars (Ex. E 215)	36	0.946	1.724	0.563	0.614			
PC 137	4	0.757	2.080	0.468	1.051			
0 V250/ M V250	3	1.728	1.639	0.132	0.554			

The s-values shown are estimates of the standard deviations of the different effects. They provide a measure of the relative influence of each effect on Road octane number.

The data were also analyzed on a laboratory-' poratory basis to provide an indication of the variation in the expects among the laboratories, and to examine effects which were independent of laboratory effects. The following table presents a summary of this analysis. Table G-2 of Appendix G gives the results in more detail.

Analysis of Variance Summary for Individual Laboratories

	No. of		Estimated Standard Deviation (s-Values)					
Lab	Cars	Cars	Fuels	Fuel x Car	Error			
3 4 5 7 8 26 29 30 35 41 47 50	4 4 3 4 5 4 4 2 2 3 7 7	0.089 0.747 0.402 1.176 0.483 1.037 0.504 0.684 0.568 2.047	1.720 1.487 2.177 1.637 1.414 1.778 1.786 2.500 1.616 1.770 1.651	0.240 0.533 0.655 0.479 0.226 0.326 * *	0.651 0.337 0.332 0.565 0.325 0.790 0.687 1.257 0.745 0.436 0.191			

^{*} The component of variance for the car-fuel interaction effect is negative and non-significant. Hence, the standard deviation is imaginary and meaningless.

^{**} Insufficient da_a for ANCVA.

The table shows that the car, fuel, and car-fuel interaction effects were similar to the all-car ANOVA. In many cases, the error standard deviations are greater than standard deviations attributable to carfuel interaction.

C. rert-Throttle Data Analysis

1. <u>Multiple Regression Analysis</u>

Equations 1-6 and 8-16 were used for regressions on the twelve-car average data. Only Equations 2, 3, and 4 gave low standard deviations, high correlations (R^2 values), and statistically significant coefficients for the variables. Regression results for these equations and Equation 5 are shown below. Results for all fifteen equations are shown in Appendix F, Table F-10. Individual car results are presented in Table F-11; Equations 1-6, 8-9, 4b, 5b, and 6b are included.

Part-Throttle Regression Equations For 12-Car Road ON Averages

Equation Model	Constant b _o	RON ^b 1	MON b ₂	Heavy Aromatics ^b 3	Ethanol b ₄	Std. Dev.	R ²
2	29.977		0.677			0.238	0.969
3	32.008	0.091	0.553			0.144	0.989
4	31.823	0.089	0.559	-0.009		0.119	0.993
5	31.740	0.086	0.562		-0.007	0.145	0.990

NOTE: Underlined value is not significant at the 95% confidence level.

As in the full-throttle results, Equation 3 was an effective predictor of Road ON. The MON coefficient was much larger than the RON coefficient, however, and in fact, MON alone was a reasonably good predictor, as shown in Equation 2.

Figure 5 graphically illustrates the good correlation using Equation 3; however, adding the percent heavy aromatics term, although very small, decreased the standard deviation from 0.144 to 0.119. The correlation is shown in Figure 6.

The table also shows results for Equation 5 which includes a term for percent ethanol in the fuels, one of the design variables. The ethanol term was very small, however, and statistically insignificant.

There were large variations in the regression results among the twelve cars tested at part-throttle. The following table shows means, standard deviations, and ranges for the twenty-fuel average ratings and the regression equation parameters (Equation 3).

Variation of Part-Throttle Road ON Regression Results Among Care

	Mean	Standard Deviation	Min.	Max.
Part-Throttle Road ON (12 Cars)	გი.035	2.197	83.805	90.75
Part-Throttle Road ON Equation Constant, b _o RON Coefficient, b ₁ MON Coefficient, b ₂	32.267 0.102 0.538	7.373 0.084 0.101	22.276 -0.050 0.406	43.611 0.230 0.770

Average Road ON values ranged from 84 to 91. The constant varied from 22 to 44, the RON coefficient from slightly negative to 0.2, and the MON coefficient from 0.4 to nearly 0.8.

2. Analysis of Variance (ANOVA)

The part-throttle data were also evaluated by ANOVA. In the part-throttle data, the car effect was the most significant factor, with 66% of the total variability. Its influence was only 20% in the full-throttle data. The fuel effect caused only 23% of the variability, and the car-fuel interaction was not significant. The ANOVA results are given in more detail in Appendix G, Table G-4.

Comparison of the part-throttle with the full-throttle ANOVA is presented in the following table.

Part-Throttle and Full-Throttle Standard Deviations

	imated d Deviation Values)	on			
Rating	No. of Cars	Cars	Fuels	Fuel x Car	Error
Full-Throttle	36	0.946	1.724	0.563	0.614
Part-Throttle	12	2.153	1.287	0.0	0.937

The most significant difference between the two data sets is that the car effect is much larger in the part-throttle fuel ratings.

D. Comparison of Results With Previous Programs

In the past, the Road Test Group has conducted fuel rating programs from which relationships for all-car averages have been developed in the form Road ON = b_0 + b_1 RON + b_2 MON. Comparison of this program's full-throttle equation with those of previous years is shown below:

1963-1980 All-Car Full-Throttle Road ON Equations

	No. of		Coeffi	cients		
	Cars	Constant*	RON	MON	Std.	2
	Tested	b _o	b	b ₂	Dev.	R^2
Program						
Premium Grade Fuels						
1964	35	14.12	0.33	0.56	-	-
1966	40	21.05	0.34	0.48	0.37	0.96
1967	14	32.04	0.01	0.71	0.63	0.90
Regular Grade Fuels		!				
1963	30	2.64	0.48	0.52	_	-
1965	36	17.15	0.32	0.53	0.68	0.84
1969	35	20.47	0.10	0.73	0.31	0.98
Unleaded Fuels						
1971	43	32.04	0.15	0.52	0.23	0.99
1973	34	2.18	0.13	0.83	0.80	0.89
1975	37	29.61	0.13	0.56	0.27	0.98
1978	34	30.94	0.31	0.36	0.21	0.99
1980	37	25.90	0.29	0.45	0.28	0.98

^{*} Constants are 'ecalculated to account for rounding off of coefficients from three-decimal form (Appendix F) to two-decimal form.

NOTE: Underlined values are not significant at the 95% confidence level.

The results of the 1980 fuel rating program show that the MON coefficient is approximately 50% higher than the RON coefficient, as compared with the 1978 program in which the RON and MON coefficients were about equal. In the other three programs conducted on unleaded fuels in 1971, 1973, and 1975, the MON coefficients were considerably higher than the RON coefficients.

In this program and in the 1978 program, the quadratic equation form which contained a $(RON)^2$ term, i.e., Road $ON = b_0 + b_1RON + b_2MON + b_6(RON)^2$, has given the best correlation because of non-linearity in fuel-rating response. In the 1975 program, however, the best equation contained a $(MON)^2$ term, i.e., Road $ON = b_0 + b_1RON + b_2MON + b_7(MON)^2$. Comparison of the full-throttle quadratic equation from this program with those of 1975 and 1978 are shown below:

1978 and 1980 All-Car Full-Throttle Quadratic Road ON Equations

ı	A) 6		Coefficients					
Program	No. of Cars Tested	Constant ^b o	RON b ₁	MON b ₂	(RON) ² b ₆	(MON) ² b ₇	Std. Dev.	R ²
1975	37	-192.167	0.146	5.789	-	-0.031	0.19	.99
1978	34	- 92.97	3.019	0.380	015	-	0.117	.997
1980	37	-143.66	3.997	0.425	020	-	0.209	.988

The negative coefficient for $(RON)^2$ in the 1978 and 1980 programs indicate that the relative importance of RON decreases as the RON level of fuels increases. In 1975, the negative coefficient for $(MON)^2$ indicates that the relative importance of MON decreases as the MON level of fuels increases. These findings are contradictory, possibly indicating that the equation form used is not the best one.

Analysis of variance of the full-throttle and part-throttle data from this program are compared below with the 1975 and 1978 programs:

1975-1980 Full-Throttle and Part-Throttle Standard Deviations

	No. of	Estimated Standard Deviation (s-Values)					
Rating	Cars	Cars	Fuels	Fuel x Car	Error		
Full-Throttle 1975 1978 1980	37 34 36	1.38 1.277 0.946	1.84 1.850 1.724	0.58 0.848 0.563	0.63 0.416 0.614		
Part-Throttle 1975 1978 1980	- 16 12	3.535 2.153	1.527 1.287	0.941 0.0	- 0.440 0.937		

In all three programs, the fuel effect accounted for most of the variability in the full-throttle data. At part-throttle, the car effect was the greatest source of variability. Car-fuel interaction was significant in the 1978 program, but not in the 1980 program.

V. DISCUSSION AND RECOMMENDATIONS FOR FUTURE PROGRAMS

Past programs have always shown significant effects of RON and MON, but no significant gasoline composition effects. This program showed that heavy aromatics adversely affects Road ON, and that ethanol gave beneficial effects in a few cars. These effects are believed to be due to imperfect fuel distribution in the intake manifold. Certain cylinders do not receive all the high-octane tail-end components such as heavy aromatics, and conversely, they may receive a higher portion of light, high-octane components such as ethanol.

This program also showed that the fuel effects vary among car models. This was demonstrated by the ethanol effect showing up in only a few cars. The findings concerning heavy aromatics and ethanol in this program are not necessarily relevant to the 1980 model car population, because the test car population is somewhat different from the 1980 car population. For example, manual transmissions and imported cars were grossly underrepresented. These car design differences may have significant effects on the cars' response to the fuel variables.

In previous programs, there has been little attempt to select test cars to represent the U.S. car population. The only effort in this direction was to recommend that select models from the octane requirement survey program be tested; however, the selection has been biased by specifying automatic transmissions. The result has been that too few imported cars and manual transmissions have been tested. It is important to have them properly represented in the test program. It is recommended that a procedure be established to assure a proper selection of test car models representing current or future vehicle populations.

Another recommendation for future programs is that fuels containing other oxygenated compounds (alcohols and ethers) be included because of the growing interest in and use of those products. Also, some type of test should be used to look at gasoline octane distribution to help explain the effects of high-octane components on Road ON.

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TABLE I

COMPARISON OF ACTUAL AND TARGET FUEL PROPERTIES

Ethanol Content, %	Actual	1	6.9	1	9.6	1	9.8	8.6	•	9.6	1	9.7	•	•	8.6	1	•	7.1	,	9.8	10.0
	Target	0	10	0	10	0	10	10	0	02	0	10	0	0	10	0	0	10	0	9	10
avy tics, %	Actua1	7.1	6.9	20.1	6.5	26.1	25.8	6.4	24.3	23.6	7.4	•	7.8	•	•	6.5	25.8	25.3	6.1	6.8	26.3
Heavy Aromatics,	Target	ស	ស	25	ល	52	25	ហ	25	25	ស	ស	ហ	25	25	ស	25	25	ស	ស	25
Z	Actual	82.5	83.4	82.7	84.6	84.3	84.4	84.7	84.8	84.1	85.7	86.2	87.5	87.2	87.3	86.3	86.7	87.7	87.6	88.4	88.9
NOW	Target	82	82	82	84	84	84	82	82	82	82	82	88	88	88	86	98	98	88	88	88
RON	Actual	90.2	89.3	91.4	90.2	90.5	90.6	95.3	95.0	94.1	95.4	93.8	94.8	94.8	94.1	1.66	•	•	98.9	•	97.9
	Target	06	06	90	06	8	06	94	94	94	94	94	94	94	94	86	86	96	86	86	86
[0]	NO.	•	~~	ო	4	വ	9	7	- α	O	10	=	12	13	14	15	16	17	18	19	20

TABLE 11

AVERAGES AND CORRELATION MATRIX OF FUEL VARIABLES

2(20 Fuels				Correlatio	Correlation Coefficient, r	nt, r	
Variable	Mean	Std. Dev.	RON	MON	Heavy Aromatics	Ethanol	(R+M)/2	Sensitivity
RON	94,535	3,298	1.000	0.784	0.035	-0.101	0.971	0.838
MON	85,750	1.899		1.000	0.083	0.129	0.910	0.318
Heavy Aromatics	15.620	9.302			1.000	-0.021	0.053	-0.021
Ethanol	4.555	4.743				1.000	-0.020	-0.268
(R+M)/2*	90.145	2.455					1.000	0.682
Sensitivity*	8.785	2.159						1.000

* Non-design fuel variable.

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ABLE III

ADDITIONAL FUEL PROPERTIES

	Aromatics, %*	20 23 23 18 30 27	38 38 30 30	25 27 28 24	27 48 34 34 28
n, °F	%06	339 311 344 341 351	312 335 336 335	308 329 352 352	350 348 331 311 351
ASTM Distillation, °F	50%	223 226 226 246 51	233 241 224 224	215 236 240 241	227 245 237 234 233
	10%	143 136 144 140	138 138 144	134 147 129	144 130 129 129
	RVP, 16	7.7.08.8.8.0 0.1.6.8.8.8.8	7.0 6.7 6.4 6.1	7.7 6.4 8.3	8.0.E.S.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8
	No.	- 0≈4₽9	7880	-2EF	15 17 19 20

* Average of data from four participants and the fuel supplier.

A CONTROL OF THE PROPERTY OF T

TABLE IV

TEST CARS

	Nodel	No.	No.	Displ.	Carb.	<u> </u>		Net
Car Code	Year	Tested	*	Liters/CuIn	ВЫ1.	Trans.	CR*	bhp
E 215	1980	i	4	1.5/90.8	2	A	8 5	67
HC5 225	1980	1	4	2.5/151	2	A	8.2	90
HIA 238	1980	1	6	3.8/231	2	A	8.0	110
HIK 238	1980	2 1	6	3.8/229	2	Α	8.6	115
HLV 225	1980	1	4	2.5/151	2	Α	8.2	86
IIF 243	1980	1	8 6	4.3/260	2 2 2 2 2 2	A	7.5	105
KI 137	1980	1	6	3.7/225		A	8.4	90
LIA 238	1980	2 1	6	3.8/231	2 V 2	Α	8.0	110
M V250	1980	1	8	5.0/302	V2	A	8.4	130
NC5 225	1980	1	4	2.5/151	2 2 4 2 2 2 2	A	8.2	90
KC7 228	1980	1	6	2.8/173	2	A	8.5	115
NFH 450	1980	1	6 8 8	5.0/305	4	A	8.6	155
NH 450	1980	1	8	5.0/305	4	A	8.6	155
NIG 230	1979	1	8	5.0/305	2	A :	8.4	130
NIJ 244	1980	1	8	4.4/267	2	Α	8.3	120
NIK 238	1980	2 1	6	3.8/229	2	Α	8.6	115
NL9 216	1981	1	4	1.6/98	2	Α	8.6	74
0 V250	1980	2	8	5.0/302	V2	A	8.4	130
OCA 133	1980	2 2	6	3.3/200	1	Α	8.6	91
OCA 223	1980	1	4	2.3/140	2 2	A	9.0	88
OCA 242	1980	2	8 8	4.2/255	2	Α	8.8	119
OI V258	1980		8	5.8/351	V2 2 1	A	8.3	140
OL 223	1980	2 4	4	2.3/140	2	Α	9.0	88
PC 137	1980	4	6	3.7/225	1	Α	8.4	90
PL 217H	1980	1	4	1.7/105	2 2 2	H	8.7	65
T 218M	1980	1	4	1.8/108	2	M	9.0	75
T 222	1980	<u> 1</u>	4	2.2/133.6	2	A	8.4	90
		37						

^{*} Manufacturer's specifications.

V = Variable venturi

TABLE Va

AVERAGE FULL- AND PART-THROTTLE ROAD OCTANE NUMBERS

	;	30 30		
Part-Throttle (12 Cars)	Max	8 8 8	O O O	999999999999999999999999999999999999999
	Min.	81.80 82.60 82.65	• • •	83.35 83.35 82.30 83.75 84.45 85.65 84.65 84.65 84.80 84.80
	Std.	2.175 1.975 1.861	1.768 2.088 1.776	2.259 2.349 2.349 2.343 1.957 2.252 2.434 2.356 2.356
	Mean	86.050 86.350 86.142		87.525 86.921 88.317 88.396 89.063 88.867 88.908 88.908 89.325 89.921 90.133
	Max.	92.45 92.30 92.00	93.50 92.25 93.50	96.30 94.70 95.15 95.15 95.00 95.70 97.15 97.45
Full-Throttle (37 Cars)	Min.	86.10 86.00 86.85	88.00 86.80 86.60	89.00 88.50 90.00 90.00 90.75 89.50 90.45 91.50
	Std. Dev.	1.028	1.067 0.919 1.433	1.355 1.329 1.201 0.943 1.298 1.442 1.442 1.447 1.447
	Mean	39	9.60	92.009 91.789 92.324 92.297 92.830 92.653 93.127 93.322 93.957 94.127
,	No.	-ae	4 w w	20 112 113 113 113 113 113 113 113 113 113

NUMBER OF ESTIMATED RATINGS

Part-Throttle	4404
Full-Throttle	∞4⊢0
Fuel	2 15 15

TABLE Vb

AVERAGE FULL- AND PART-THROTTLE ROAD OCTANE NUMBERS

	Max.	88.25 88.25 88.25 88.60 89.05	90.85 90.55 89.75 91.35 91.20 92.45 91.90	92.00 92.25 92.25 92.25 93.00
Part-Throttle (8 Cars)	Min.	83.00 83.45 83.45 84.25 84.25	84.50 84.70 83.70 85.45 85.35 85.90 85.70	85.45 85.65 85.90 86.70 86.75
	Dev.	2.009 1.829 1.822 1.454 1.971	2.183 2.231 2.025 2.025 2.160 2.334 1.886	2.188 2.275 2.212 2.241 2.156
ď	Mean	86.144 86.388 86.250 86.888 86.725	87.638 87.656 87.044 88.294 88.506 89.125 88.763	88.894 88.900 89.350 89.650 90.025
Full-Throttle (26 Cars)	Max.	89.90 90.70 91.25 91.60 90.65	94.00 93.60 92.65 93.30 93.70 94.05	94.50 95.45 95.75 95.50 96.40
	Min.	86.10 86.00 86.85 88.00 86.80	89.00 89.00 88.50 89.95 90.00 91.20 90.75	89.50 90.45 90.50 91.50 91.50
	Dev.	0.959 0.851 0.843 0.775 0.768	1.065 1.109 1.036 0.998 0.773 0.854 1.045	1.295 1.264 1.349 1.020 1.205
	Mean	88.935 89.123 89.421 89.744 89.446	91.710 91.525 91.077 91.992 92.110 92.587 92.527	92.881 93.108 93.385 93.577 93.819
,	No.	− ∨ ≈ ± ъ o	7 8 8 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	15 17 18 19 20

-23-<u>TABLE VI</u>

REGRESSION EQUATIONS

General Model: Road ON = b_0+b_1 %ON+ b_2 MON+ b_3 HVYA+ b_4 ETOH+ b_5 (R+M)/2+ b_6 (RON)²+ b_7 (MON)²+ b_8 RXM

Eqn. No.	Constant b _O	RON b ₁	MON b ₂	Heavy Aromatics b ₃	Ethanol b ₄	(R+M)/2 b ₅	(RON) ²	(MON) ²	RON×MON b ₈
1	X	χ							
2	X	^	v						
3	X	Х	X						
4	X	X	X	х					
4a*	X	X	^	X					
4b*	X	^	Х	X					
5	X	Х	×	^	X				
5a*	X	X	^		X				
5b*	X	^	Х		X				
6	X	Х	X	Х	X				
6a*	X	X	^	х х	X				
6b*	X	·	Х	X	X				
7	X			,	^	Х	1		
8	X	Х	Х			^	x		
9	X	X	X				"	X	
10	X	Х	Х	х			x		
11	X	Х	X		χ		X		
12	X	Х	X	Х			"	X	
13	X	Х	X		Х			X	
14	X	Х	Х	x	Х		X	-	
15	χ	Х	Х	Х	. х			X	
16	χ	Х	Х				X	X	X
17	X	Х	Х	х			x	x	x
18	Х	Х	Х		Х		X	Х	X
19		Х	χ	х	Х		х	X	Х
20	X X	Х					X		
21			Х					X	
22	X X	Х		х			x		
23	X	Х			Х		X		

 $[\]star$ For individual cars there were twelve Equation 3 regressions for which either RON or MON was not a significant variable. These equations were used for those FT or PT cases.

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TABLE VII

LINEARIZED RON, MON, (RON)² EQUATION*

(37-Car Average Full-Throttle Road Octane Ratings)

$\frac{b_2'}{(b_1' + b_2')}$	0.455	0.4/3	0.497	0.520	0.547	0.576	0.608	0.645	0.685	, Cr C	0.731	0.784
b ₁ + b ₂	0.934	0.895	0.855	0.816	0.777	0.748	0.699	0.659	0.620		0.581	0.542
MON b2'	0.425	0.425	0.425	0.425	0.425	0.425	0.425	0.425	0.425	011	0.425	0.425
RON b1	0.509	0.470	0.430	0.391	0.352	0.313	0.274	0.234	101.0	0.130	0.156	0.117
Constant b ' 0	8.141	11.631	15.251	18.820	22 428	26.1ES	20.02	22.226	030.00	37.344	41,147	44.989
RON	89	06	5	- 00	7 0	5 K	+ 5	2 (D (6	ă	66

* To Convert Second Order Road ON Equation (1)

(1) Road ON = $b_0 + b_1 RON + b_2 MON + b_6 (RON)^2$

To Linearized Form (2)

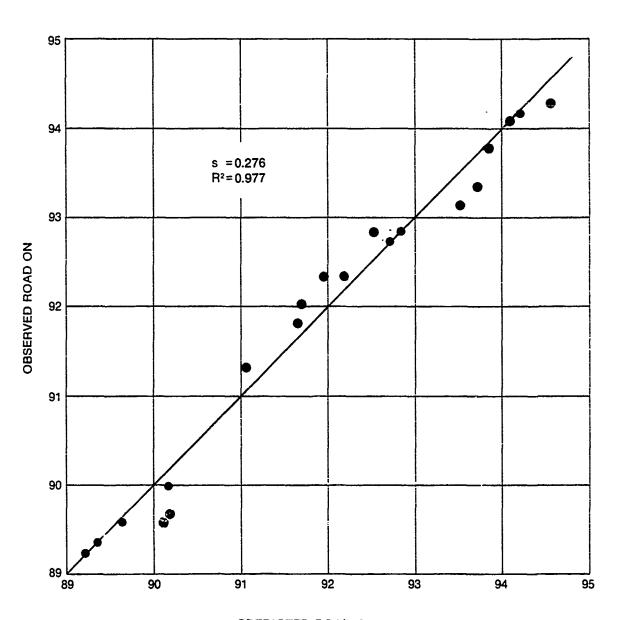
(2) Road ON = b_0 ' + b_1 'RON + b_2 'MON

As Follows:

$$b_1' = (\frac{-Road\ ON}{-RON})_{MON} = b_1 + 2b_6RON$$
 $b_2' = (\frac{-Road\ ON}{-MON})_{RON} = b_2$
 $b_0' = Road\ ON - b_1'ROM - b_2'MON$

Figure 1

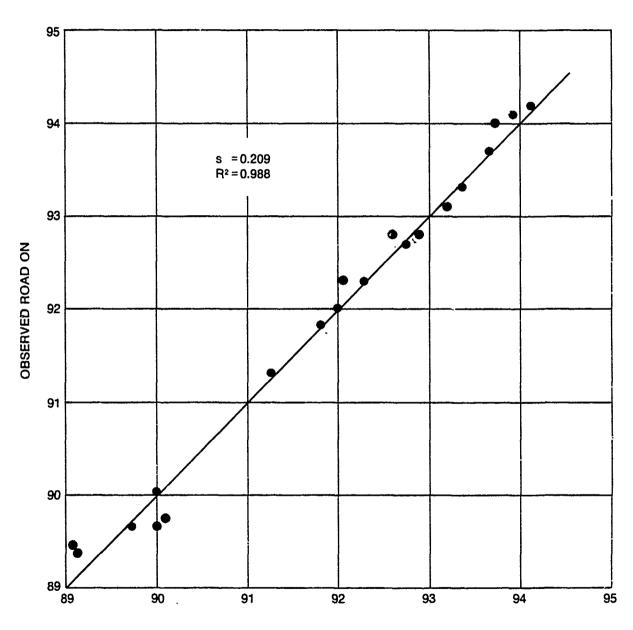
PREDICTION OF 37-CAR AVERAGE FULL-THROTTLE ROAD ON BY RON, MON EQUATION



PREDICTED ROAD ON
ROAD ON = 26.275 + 0.286 RON + 0.450 MON

Figure 2

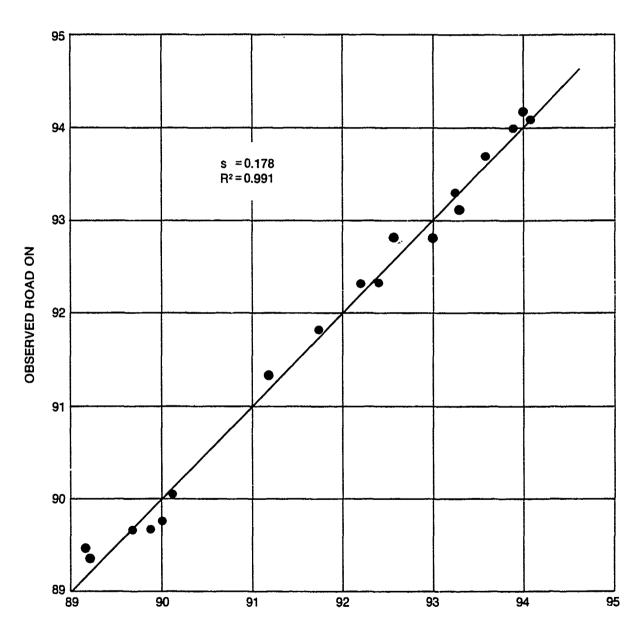
PREDICTION OF 37-CAR AVERAGE FULL-THROTTLE ROAD ON BY RON, MON, (RON)² EQUATION



PREDICTED ROAD ON ROAD ON = $143.663 + 3.997 \text{ RON} + 0.425 \text{ MON} - 0.020 (RON)^2$

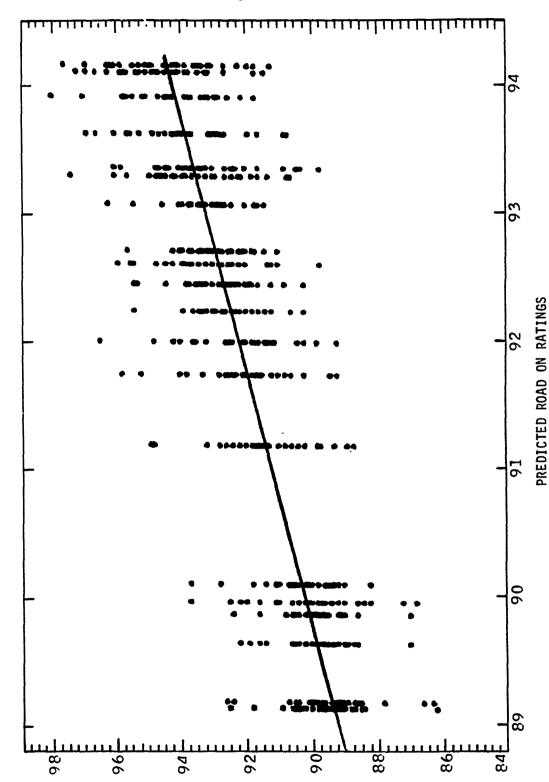
Figure 3

PREDICTION OF 37-CAR AVERAGE FULL-THROTTLE
ROAD ON BY RON, MON, (RON), HEAVY AROMATICS EQUATION



PREDICTED ROAD ON ROAD ON = -163.216 + 4.294 RON + 0.432 MON -0.021 (RON)² -0.012 HEAVY AROMATICS

Figure 4



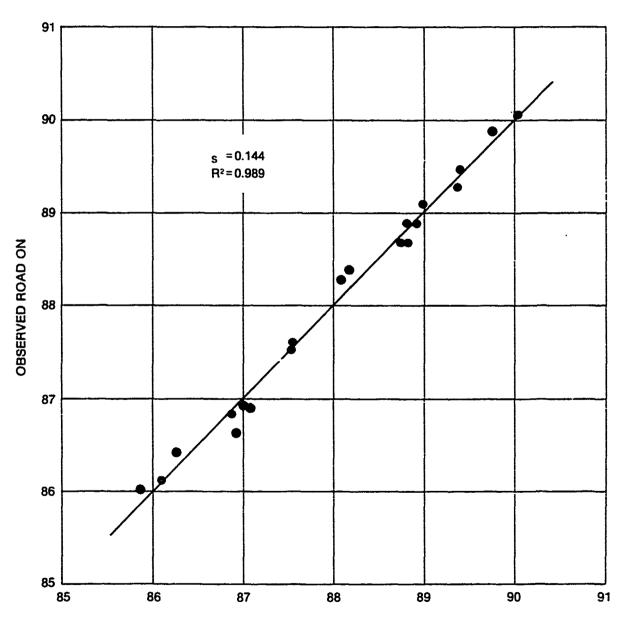
ROAD ON RATINGS BY SINGLE REGRESSION EQUATION

PREDICTION OF 37 INDIVIDUAL FULL-THROTTLE

ROAD ON = -165.815 + 4.317 RON + 0.437 MON - 0.021 (RON)² - 0.012 HEAVY AROMATICS

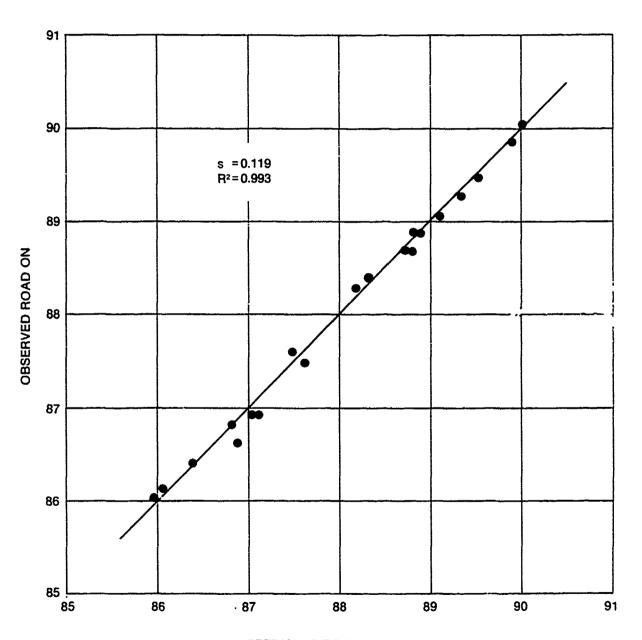
OBSERVED INDIVIDUAL CAR ROAD ON RATINGS

Figure 5
PREDICTION OF 12-CAR AVEF AGE PART-THROTTLE
ROAD ON BY RON, MON EQUATION



PREDICTED ROAD ON
ROAD ON = 32.008 + 0.091 RON + 0.553 MON

Figure 6
PREDICTION OF 12-CAR AVERAGE PART-THROTTLE
ROAD ON BY RON, MON, HEAVY AROMATICS EQUATION



PREDICTED ROAD ON

ROAD ON = 31.823 + 0.089 RON + 0.559 MON - 0.009 HEAVY AROMATICS

A P P E N D I X A

PARTICIPATING LABORATORIES

AND

MEMBERSHIP OF ANALYSIS PANEL

PARTICIPATING LABORATORIES

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Chevron Research Company
E. I. du Pont de Nemours & Company, Inc.
E.R.I.
Gulf Research and Development Company
Mobil Research and Development Corporation
Shell Development Company
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Suntech, Inc.
Texaco Inc.
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Union Oil Company of California

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Gulf Research and Development Company

Shell Development Company

Supplied laboratory inspection data only.

APPENDIX E

PROGRAM

1980 FUEL RATING PROGRAM:

ROAD OCTANE PERFORMANCE IN 1980 MODEL CARS

CRC Project No. CM-124-80

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IV. FUELS (UNLEADED)	B-6
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FICURE 2 - Took Evol Docion	R_11

PROPOSED 1980 FUEL RATING PROGRAM ROAD OCTANE PERFORMANCE IN 1980 MODEL CARS

I. Forward

Road octane rating programs have been conducted periodically by the CRC Motor Road Test Group to investigate the relationship between the laboratory properties of a set of motor gasolines and the road anti-knock performance of these fuels in a selected group of cars. Leaded gasolines were employed during the 1963-1969 period. The programs of 1971, 1973, and 1975 involved unleaded fuels; the 1975 and 1978 programs were run with cars equipped with catalytic converters. The testing was done by Road Test Group participants from the oil and automobile industries at their own laboratories.

II. Objective

In past programs total aromatics and olefins contents have been evaluated for possible effects on road octane performance, and their effects have been found to be statistically nonsignificant. However, heavy aromatics may be a significant factor affecting Road octane number. Another gasoline variable of interest is ethanol content, since ethanol is used in "gasohol" blends being widely distributed. The objective of this program is to evaluate these variables along with Research octane number (RON) and Motor octane number (MON) in 1980 model cars.

. III. Test Cars

The desire is to test the fuels in a population of cars representative of the 1980 models that will be on the road. In order to do this, a variety of car and engine models is required. However, because of the size limitation of the program, low sales volume models should not be tested. Models with manual transmissions should be included, however, because they constitute a significant portion of new car sales.

Engines of cars used for road rating of the fuels in this program should not be altered from their factory configuration except as necessary for instrumentation required for the Modified Uniontown technique. The cars should have at least 6000 miles and maximum octane requirements (CRC E-15 Technique) of at least 86 RON with 1979

or 1986 FBRU fuels. Cars used for part-throttle ratings should have part-throttle octane requirements of 86 RON FBRU minimum. In addition, spark timing should not exceed the following limits when rating any of the test fuels: 10 degrees retarded to 15 degrees advanced, relative to manufacturer's recommended basic timing.

IV. Fuels (Unleaded)

Fuel variables to be investigated are RON, MON, heavy aromatics (c_9+) , and ethanol content. A computer optimization program was used to design a test fuel set of 20. The optimization provided for the evaluation of $(RON)^2$ and $(MON)^2$ effects in addition to linear effects for the four variables. Small second-order effects were found for RON and MON in the 1978 program, but second-order effects are not expected for heavy aromatics or ethanol content.

Table I and Figures 1 and 2 show the fractional factorial design of the test fuel set. Because only linear effects are expected for heavy aromatics and ethanol content, only low and high values are used; intermediate values are not needed. Five levels of MON and three levels of RON are required to evaluate both linear and second-order effects. Normally only three levels are needed to assess nonlinearity of a variable. However, because sensitivity was constrained to 6-12 ON for all fuels, the combinations of RON and MON were limited, as shown in Figure 1. In this situation more than three levels of MON are required for an optimum test fuel set.

Test fuel specifications are shown in Table II. Samples of the test fuels will be sent to the participants for octane, hydrocarbon composition, distillation, and Reid vapor pressure data.

V. Test Procedure

All fuels are to be rated in duplicate in each car by the Modified Uniontown (CRC Designation F-28-70) technique. Ratings are to be obtained at full throttle (maximum or wide open) and at the most critical part-throttle condition occurring with manifold vacuum of 4 in. Hg or greater above the full throttle vacuum. However, part-throttle tests should not be conducted if ratings cannot be determined on all design fuels without exceeding the spark advance limits. Part-throttle ratings must be determined from part-throttle primary reference fuel curves.

At least three accelerations should be made for each rating. The fuels should be rated in a random order. The maximum speed investigated for Modified Uniontown rating should not exceed 60 mph.

VI. Data Reporting

Data should be reported to CRC prior to December 1, 1980, using data forms to be provided. To aid in analysis, each participant is requested to report the manufact rer's recommended ignition timing for the cars and the spark advance (t idle speed) for each Modified Uniontown fuel rating. If spark advance is read at other than idle speed, the data should be corrected to idle speed for reporting on the data forms. Other important details to be reported are transmission gear for full throttle ratings, manifold vacuum for part-throttle ratings, and complete car information as indicated on the data forms.

In all cases, each participant is requested to report data for all items included on the data report forms. To assure legible copies, each participant is requested to use a soft pencil or black ink when completing the data forms in longhand.

VII. <u>Data Analysis</u>

Analyses will be conducted on both full throttle and part-throttle data. Other subgroups of data that will be analyzed are all car averages, model averages, individual cars, and individual laboratories. Linear and second-order equations will be developed using RON, (RON)², MON, (MON)², heavy aromatics, and ethanol content as the variables. Analysis of variance (ANOVA) techniques will be used to evaluate individual contributions of cars, fuels, car-fuel interactions, and test error to the variability of the Road octane ratings.

TABLE I
TEST FUEL DESIGN

Fuel				Heavy	
No.	RON	MON	Sensitivity	Aromatics*	Ethanol*
12345678901123456789011234567890	99999999999999999999999999999999999999	222444222558886666888 888888888888888888888888	8 8 8 6 6 12 12 12 12 12 10 10 10	55555555555555555555555555555555555555	0 10 0 10 10 10 0 10 0 10 0 10 0 10 0

^{*}Percent by volume.

TABLE II

TEST FUEL SPECIFICATIONS

Octanes

Meet the specified octanes within ± 0.5 ON.

Heavy Aromatics

Meet the specified C_9 and heavier aromatics contents within $\pm 2\%$ by volume.

Ethanol

Meet the specified ethanol contents within $\pm 0.5\%$ by volume. Ethanol must be at least 198-proof CDA-19 or CDA-20.

Volatility

Reid Vapor Pressure	-	8-10 Lb
ASTM D 86 Distillation		
IBP		90°F Minimum
10% Evaporated	_	110-150°F
30% Evaporated	_	140-195°F
50% Evaporated	_	180-260°F
70% Evaporated		220-310°F
90% Evaporated	_	285-380°F
EP	_	450°F Maximum

Other

Total Aromatics Content- 10-50% Total Olefins Content - 0-25%

Benzene Content - 1% Maximum

Lead Content - 0.03 g/Gal. Maximum

Sulfur Content - 0.05% Maximum

Manganese - None to be Added

Antioxidant - 5 PTB (100% Active)

Blending Components - Normal Refinery Components

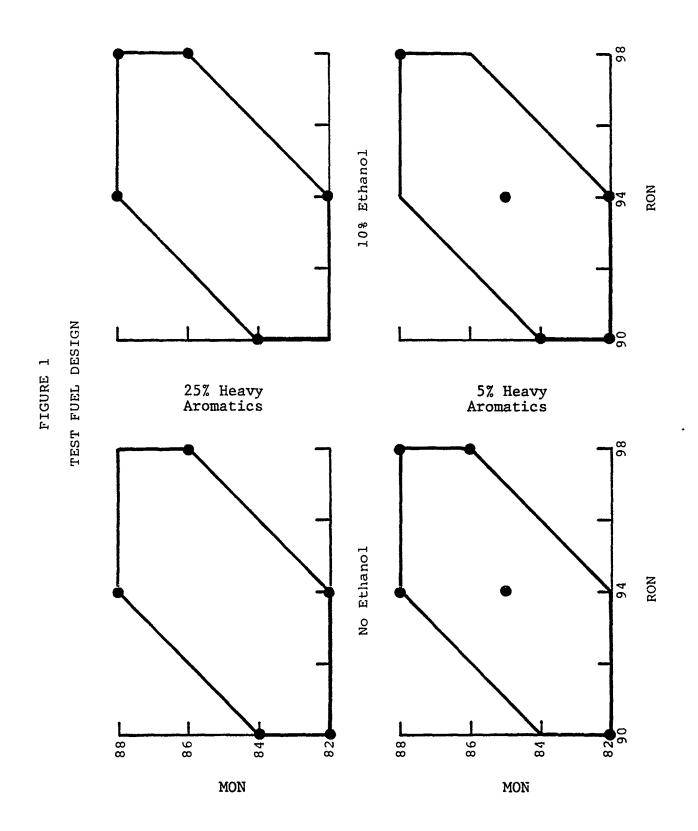
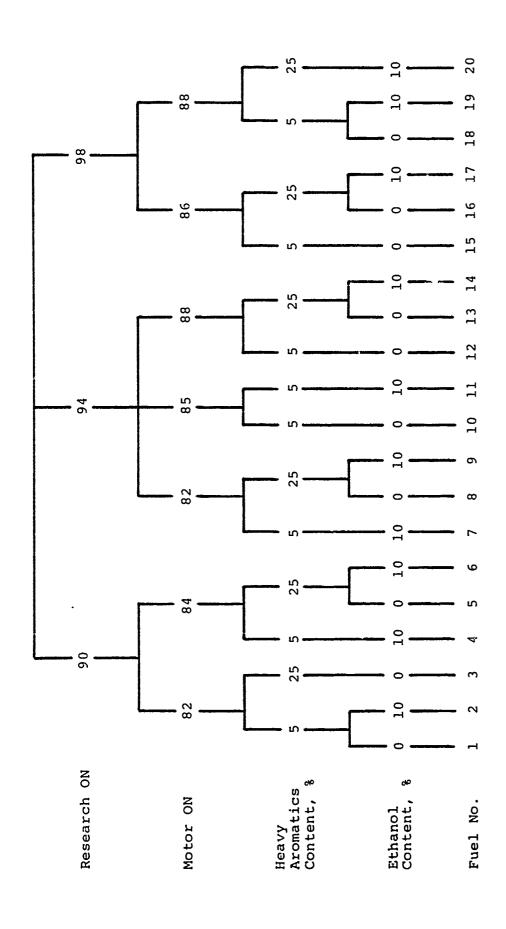


FIGURE ? TEST FUEL DESIGN



APPENDIX C

CAR-LABORATORY TESTING ARRAY

CAR-LABORATORY TESTING ARRAY

LIA 238			8	2		2	2
KI 137		-		_			
IIF 243			-	_			
HLV 225	UNIONTOWN		-	-	UNIONTOWN		
HIK 238	FULL-THROTTLE MODIFIED UNIONTOWN	-	-	2	PART-THROTTLE MODIFIED UNIONTOWN		
HIA 238	FULL-THRO	-		-	PART-THRO		
HC5 225		-		-			
Car Code:	Laboratory	ω 4 υ∕ω(26 33 34 50 50	Total	4	2 7 2 2 5 2 6 2 6 2 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9	Total

ARRAY
TESTING
-LABORATORY
CAR

NIJ 244		-	-			
NIG 230*		~	-			
NH 450		-	-			
NFH 450	D UNIONTOWN		-	D UNIONTOWN		
NC7 228	FULL-THROTTLE MODIFIED UNIONTOWN	-	-	PART-THROTTLE MODIFIED UNIONTOWN		
NC5 225	FULL-THR	-	-	PART-THE	-	-
M V250		-	-			
Car Code:	Laboratory	8 4 5 7 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	oc Total		29 7 5 7 5 4	Total

* 1979 Mode

CAR-LABORATORY TESTING ARRAY

01 V258	-	-	- -
0CA 242		2	2
0CA 223	-	_	
0CA 133	UNIONTOWN 2	2 UNIONTOWN	2 2
0 7250	FULL-THROTTLE MODIFIED UNIONTOWN 1 2	1 2 2 PART-THROTTLE MODIFIED UNIONTOWN	
NL9 216**	FULL-THROT	1 PART-THROT	- -
NIK 238		7	
Car Code:	Laboratory 3 4 5 7 29 30 41 47	Total	4 5 7 29 Total

** 1981 Model

CAR-LABORATORY TESTING ARRAY

TOTALS		ቀ ቀመ	4 N	ব ব	~~	m – –	37		w-44	12
T 222							-			
T 218M	N.					-	-	N.		
E 215	IED UNIONTO					-	- -	FIED UNIONTO		
PL 217M	FULL-THROTTLE MODIFIED UNIONTOWN					-	_	PART-THROTTLE MODIFIED UNIONTOWN		
PC 137	FULL-TH		-	~	8		4	PART-TI	-	_
0L 223		-	~				2		-	-
Car Code:	Laboratory	w 4	2 /	8 26	30 30	35 41 47	50 Total		420	29 Total

APPENDIX D

MODIFIED UNIONTOWN TECHNIQUE (CRC DESIGNATION F-28-70)

INDEX OF APPENDIX D

MODIFIED UNIONTOWN TECHNIQUE (CRC Designation F-28-70)

Scope Vehicle Preparation for Test Instrumentation Reference Fuels Test Procedure Report and Interpretation of Data

MODIFIED UNIONTOWN TECHNIQUE

(CRC Designation F-28-70)

This research technique has been developed for research purposes only and is not to be construed as a specification or standard, since the Coord_nating Research Council, Inc. does not promulgate specifications or standards.

Prepared by the

Road Rating Techniques Study Panel

of the

CRC-Motor Road Test Group

June 1970

Revised: October 1975

A. SCOPE

The Modified Uniontown Test Technique is designed to determine a single road octane rating of a gasoline under level road accelerating conditions. The ratings are generally made at maximum throttle but may be made at part throttle if desired or more critical. It is under these relatively severe conditions that the motoring public would probably encounter knock and thus be able to compare or evalute fuel octane quality.

The Modified Uniontown Technique employs the vehicle's standard spark advance mechanism. The basic spark setting is varied until trace knock is obtained during acceleration for the primary reference fuel series and the gasoline(s) being rated. Trace knock is the lowest level of knock intensity that can be heard repeatedly.

The Modified Uniontown rating of a gasoline is the octane number of the PRF blend which would be expected to produce trace knock at the same basic spark advance as the test gasoline.

B. VEHICLE PREPARATION FOR TEST

The mechanical checks given below should be made as indicated. All adjustments should be made to conform with manufacturers' specifications unless—herwise specified in this section.

- (1) Procurement checks: The checks listed below should be made upon initial receipt of vehicle for test. The vehicle should have accumulated sufficient mileage to provide adequate break-in and achieve deposit accumulation.
 - (a) Compression pressures should be checked according to manufacturers' recommended procedures,
 - (b) Check timing mark vs TDC on cylinder number one piston, using a dial gage or equivalent.
 - (c) Carburetors should be in good operating condition. If the vehicle is to be used for fuel rating for an extended period of time, it is recommended that carburetor mixture checks be made periodically to assure that the carburetor remains in the as-received condition.
 - (d) Check the tappet clearance against manufacturers' specification and adjust to limits.

B. VEHICLE PREPARATION FOR TEST (Cont'd)

- (e) Install new set of spark plugs of recommended heat range (preferably after the deposit stabilization accelerations described in E2b). For continued high-speed operation, colder plugs may be desirable.
- (f) Check distributor automatic spark advance mechanism for conformance to manufacturer's recommended specifications.
- (g) Check fuel pump as per manufacturer's recommended procedure. Replace fuel filter element.
- (h) Observe choke plate and make certain it is in wide-open position with the engine fully warmed up. Wire open automatic choke if necessary.
- (i) Check throttle opening linkage for true wide-open throttle position, freedom from sticking, etc.
- (j) Check heat valve to determine if it is free and operating normally. Allow it to function as in normal driving operation.
- (k) Check crankcase breather or emission control system to insure satisfactory operation. Check air cleaner element and replace if necessary.
- (1) Check the exhaust emission control system for proper operation.
- (m) Check the fuel system evaporative control system, and also deactivate the fuel recirculating system, if so equipped, to obviate the possibility of flooding the fuel system.
- (n) Check the operating temperature of the coolant thermostat to ascertain if it is operating correctly.
- (o) Check the automatic transmission's shift characteristics for conformance with manufacturers' specifications.
- (p) Check all belts for tightness and condition.
- (2) Daily checks: The daily checks should include the items listed as (h), (i) and (j) in Paragraph (l) above, and also items listed below.
 - (a) Check tire pressure.
 - (b) Check oil level.
 - (c) Check coolant level and note type and freezing point of coolant used.

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B. VEHICLE PREPARATION FOR TEST (Cont'd)

- (d) Operate the vehicle to test general performance characteristics, misfiring, surging, excessive noise, etc. A check of vehicle acceleration time under standard rating conditions at manufacturers' recommended spark timing would provide a good indication of overall vehicle performance.
- (e) Check brakes for safe operating and reserve pedal.
- (f) Make a visual check of the engine compartment just before start of test and periodically during testing to observe general mechanical condition of the engine. Look for water, oil and gasoline leaks, or any other sign of malfunctioning.
- (3) Weekly or 1000 mile checks: Weekly or 1000 mile checks should include items (a), (i); (j), and (k) in paragraph (1) above, and also items listed below.
 - (a) Check auxiliary fuel systems for leaks, particularly if valving is used that might permit contamination of test or reference fuels.
 - (b) Check spark plugs for misfiring and gap to manufacturers' recommended procedures.

C. INSTRUMENTATION

- (1) Spark Advance Measurement: A method of accurately measuring basic spark timing should be provided. This can be done either mechanically or electronically. The equipment should be:
 - (a) Convenient to read from the passenger compartment during normal vehicle operation, unless remotely indicated or recorded.
 - (b) Capable of indicating spark timing within + 1/2 crank-angle degree.
 - (c) Unaffected by the vibrations, accelerations, or shock normal to full throttle vehicle acceleration.
- (2) Spark Advance Centrol: A mechanism should be provided to control spark advance from the passenger compartment. This control should be positive, with a minium of hunting or backlash, and should not be affected by engine movement due to torque reaction.

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C. INSTRUMENTATION (Cont'd)

- (3) Engine Speed Measurement: A method of measuring engine revolutions per minute should be provided which is:
 - (a) Capable of instantaneous reading and/or recording throughout the engine speed range.
 - (b) Convenient for reading from the passenger compartment during vehicle operation.
 - (c) Capable of indicating within an accuracy of ± 50 rpm and with a repeatability of $\pm 1\%$ of the speed being read.
 - (d) Unaffected by the vibrations, accelerations, or shock normal to full throttle vehicle accelerations.
- (4) Manifold Vacuum Measurement: A vacuum gage should be connected to the intake manifold and located where it can be seen by the driver. This is important for automatic transmission test cars in order that the car can be driven repeatably at a low engine speed and at as low a manifold vacuum as possible without automatic downshifting to a lower gear.
- (5) Temperature Measurement: While temperature measurements are not directly necessary for fuel rating, they are important for checking the general operation of the engine and for controlling the operating conditions of the car when it is used on successive occasions. It is, therefore, suggested that thermocouples be installed in the following locations and the suitable instrumentation be provided to measure or record the following temperatures:
 - (a) Carburetor inlet air
 - (b) Engine coolant (block exit)
 - (c) Engine oil (sump or gallery)
 - (d) Automatic transmission oil
 - (e) Intake mixture (after stove area)
- (6) Weather Measurements: It is suggested that the following ambient weather conditions be measured and recorded hourly during fuel rating tests:
 - (a) Temperature
 - (b) Humidity
 - (c) Barometric pressure

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C. INSTRUMENTATION (Cont'd)

(7) Auxiliary Fuel System: An auxiliary fuel system should be provided to facilitate convenient switching from one fuel to another. The auxiliary fuel line should be connected to the inlet side of the fuel pump, should be of minimum length, and should be routed in such a way as to avoid trapping fuel vapor. Installation should give consideration to safety as well as convenience of fuel handling. To minimize mixing of test fuels during fuel change-over it is recommended that fuel settling bowls or large filters be blocked off and/or replaced by small filter assembly with the bowl mounted in an inverted position.

If an electric fuel pump is used, the fuel pressure at the carburetor should be checked to conform with the manufacturers' recommendation.

For cars used extensively for fuel ratings, carburetor bowl drain lines connected to a pump and waste can have been found to improve the speed and completeness of fuel system draining when changing from one fuel to another.

D. REFERENCE FUELS

Primary reference fuel blends should be prepared in two octane number increments over the range required to bracket the fuels being rated.

E. TEST PROCEDURE

(1) Engine Warmup

To stabilize engine temperatures, a minimum of fifteen miles of operation under road load conditions at speeds of 50 to 60 mph in top gear is required.

- (2) Combustion Chamber Deposits Stabilization
 - (a) Cars should have a minimum of 2000 deposit miles prior to use for road octane rating. The last 500 miles should be accumulated under medium to high speed conditions to insure stabilization of combustion chamber deposits.
 - (b) Just prior to conducting each series of road octane rating tests, the following deposit stabilization run should be made:
 - (1) With the vehicle fully warmed up, set the spark timing to produce approximately light knock on tank fuel or other fuel which knocks near the manufacturers' recommended spark setting. (Knock should cover the expected range of testing.)

E. TEST PROCEDURE (Cont'd)

- (2) At the above spark setting make several accelerations over the speed range in which road ratings are desired. The accelerations should be conducted primarily at wide-open throttle employing part throttle only as required to limit maximum knock to light intensity.
- (3) Fuel Changeover
 - (a) Catalytic Device Cars

Caution: Because of the installation of catalytic devices on these cars, permanent damage may result if the engine runs over lean or stalls. Therefore, changeover from one fuel to another must be accomplished without running the carburetor dry.

To eliminate contamination of the new fuel with residual amounts of the previous fuel, the car will be operated under the following conditions after charging with the new fuel: operate car for 2 miles at a maximum speed of 55 mph during which time four part-throttle accelerations at approximately 4" Hg manifold vacuum are made.

- (b) Non-catalytic device cars or catalytic device cars for which the manufacturer has provided written approval to run the carburetor dry with assurance the procedure will not damage the catalytic device.
 - (1) With one and two-barrel carburetors, the carburetor shall be run dry at 55 mph, road load, in highest gear.
 - (2) With four-barrel carburetors, the primary float chamber shall be run dry at 55 mph, road load, in highest gear. The secondary float chamber shall be run dry by going to wide-open throttle for short periods of time, being careful to avoid excessively high engine speeds. This must be accomplished in passing gear on those vehicles in which the secondary throttle plates are mechanically actuated by depressing the throttle beyond the detent position.

Caution: In cars equipped with automatic transmissions, care should be taken to maintain the car speed sufficiently high to keep the engine turning over. This is especially important to cars equipped with power brakes since a serious safety hazard may be encountered with a dead engine.

- (c) Charge the fuel system with a new test fuel and repeat the operations described in paragraphs (a) or (b).
- (d) After fuel changeover, make one preliminary acceleration before beginning Vehicle Rating Procedure and operate one-half mile at 50 to 60 mph, road load, to obtain stabilized conditions.
- (4) Operating Conditions
 - (a) The vehicles should be tested at or as near maximum throttle as possible over the widest practicable speed range.

In the case of manual transmissions, this is wide-open throttle in top gear.

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E. TEST PROCEDURE (Cont'd)

In the case of automatic transmissions, it is dependent upon the transmission control system and may vary considerably among car makes. Operating characteristics of each vehicle should be explored to determine the drive ratio which will allow operation at or near wide-open throttle over the widest range of engine speed.

- (b) Fuel ratings should be run on a smooth, level, straight road in either direction as long as audibility of knock is not affected by the wind. Tests shall not be conducted during periods of rain or rapidly changing weather conditions. Fuel ratings may also be run on a chassis dynamometer with proven good road correlation.
- (c) Care should be taken not to operate at greater than light knock intensity because of the effect on combustion chamber temperatures and knock intensity during the remainder of the acceleration.
- (d) Excessively advanced or retarded ignition timings may lead to abnormal fuel ratings. Where possible, road rating determinations should be made within the range of 15 degrees advance to 10 degrees retard from the manufacturers' standard spark advance (recommended basic ignition timing plus centrifugal spark advance) at any speed.
- (e) The speed range investigated will normally extend to 3000 rpm, but where conditions necessitate should be extended beyond.

(5) Details of Observations

(a) The vehicles should be accelerated from as low a speed as practicable to as high a speed as desired. For manual transmission cars the acceleration should be made in highest gear from the lowest speed giving reasonably smooth operation; the minimum engine speed will normally be about 700 rpm.

In the case of automatic transmission cars, the critical rating condition is dependent upon the transmission control system and may vary considerably among car makes. Operating characteristics of each vehicle should be explored to determine the drive ratio and throttle position which will allow operation at or near wide-open throttle over the widest range of engine speed with the gear selector in <u>Drive</u> position. It may be expedient to decrease intake manifold vacuum during the acceleration in accordance with a schedule predetermined for the particular test car.

E. TEST PROCEDURE (Cont'd)

- (b) Adjust basic spark timing to produce knock of trace intensity over as narrow a speed range as possible during the acceleration. Trace knock is defined as the lowest level of knock that is readily and constantly discernible to the ear. It is NOT the threshold between knock and no knock. Generally, the spark setting should not be changed during an acceleration except when encountering heavy knock. All comparative tests with different fuels must be made at the same trace knock intensity over the same speed range, recognizing that all fuels may not knock in the same portion of the speed range.
- (c) Subsequent accelerations should be spaced at relatively constant time increments in order that repeatability of testing conditions is assured. Excessive braking between accelerations should not be utilized as temperature equilibria may not be reached before each successive acceleration is commenced. Experience with a particular vehicle and/or testing condition may dictate otherwise, but a time period of approximately 20 seconds between successive accelerations with several seconds at constant speed before the start of each acceleration is considered satisfactory to yield reproducible results.
- (d) The first one or more accelerations is exploratory, to enable the operator to become acquainted with the knocking characteristics of the fuel. At least two accelerations are made for recording of data. Basic spark advances required for trace knock intensity are recorded with the corresponding speed range of knocking.
- (e) With adequate instrumentation and adherence to procedural details, basic spark advances for trace knock accelerations generally will not differ more than one crankshaft degree. In such instances, two trace knock accelerations shall suffice and the average of the spark settings for the two accelerations shall be reported for the fuel.

If the spark advances for the first two trace knock accelerations will differ by more than one degree, one or more additional accelerations shall be made as required to establish a good average spark setting.

(f) It is recommended that at least four different reference fuels be rate to establish a reference fuel framework before running the test gasolines. Additional reference fuels should be interspersed with the test gasolines to complete the reference fuel framework in two octane number increments. Several reference fuels should be rechecked at intervals

F. REPORT AND INTERPRETATION OF DATA (1)

- (1) Calculate average basic spark advance for each fuel. Where rechecks have been run, use all valid spark advance observations.
- (2) Establish basic spark advance vs octane number curve for reference fuels.
- (3) Obtain the octane number rating of each test gasoline by determining the octane number corresponding to the average basic spark advance value. The octane number is reported with the speed of maximum knock.
- (4) The reproducibility⁽²⁾ of the Modified Uniontown Road Octane Number Test has been found to be about one octane number. Therefore it is recommended that when the result of a single determination is to be reported it should be rounded off to the nearest 0.5 number. However, when multiple ratings are obtained, these individual ratings sho of the rounded off, but the average may or may not be, depending on the individual laboratory's testing errors, and the ultimate utilization of the rating number.
- (1) All calculations described herein may be accomplished either manually or by E.D.P. (electronic data process).
- (2) Reproducibility is a quantitative expression of the random error associated with single determinations at "ifferent laboratories of a property of an identical material utilizing the same method. It represents the maximum difference between such measurements which would be expected to be exceeded in a given percentage of cases

The reproducibility figures quoted above are calculated for one standard deviation which is normally exceeded in about 30% of the cases. Reproducibility is currently defined as the square root of the total testing variance usinus the fuel variance.

(It must be noted that this reproducibility figure does not correspond to that of ASTM which is normally exceeded in only one case out of 20.)

APPENDIX E

AVERAGE ROAD OCTANE RATINGS
MODIFIED UNIONTOWN TECHNIQUE

INDEX OF APPENDIX E

Index of Tables

Table E-1 Average Road Octane Ratings

Full-Throttle Road ON

By Car Model

Table E-2 Average Road Octane Ratings

Full-Throttle Road OH

For Each Car

Table E-3 Average Road Octane Ratings

Part-Throttle Road ON

For Each Car

TABLE E-1

AVERAGE FULL-THROTTLE ROAD OCTANE NUMBER RATINGS

Population Averages

Population:	All Imports*	PC 137*	0 V250/M V250*
No. of Cars	3	4	3
Fuel No.			
1	89.9	88.0	90.6
2	(89.9)	(89.6)	(90.4)
3	89.8	90.1	90.2
4	90.8	89.6	91.0
5	90.0	89.2	99.4
6	89.9	91.0	91.0
7	92.9	(92.6)	(92.8)
8	92.1	92.0	93.2
9	91.8	91.9	92.5
10	92.6	92.6	93.2
11	91.9	92.8	93.0
12	93.4	92.6	94.0
13	92.6	92.6	93.5
14	93.4	93.6	93.5
15	(93.0)	93.9	93.9
16	93.0	93.8	94.6
17	(93.8)	(94.9)	(94.3)
រិទ	94.8	94.6	94.6
19	94.8	95.1	94.9
20	94.7	95.3	94.8

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-2

AVERAGE FULL-THROTTLE ROAD OCTANE NUMBER RATINGS

Individual Cars

Car Code: <u>HC5 225</u> <u>HIA 238</u> <u>HIK 238</u> <u>HIK 238</u> *	HLV 225*
Car Number: 2 13 4 27	30
Laboratory: 3 8 3 35	41
Fuel No.	
1 89.4 89.0 89.8 90.2	88.1
2 90.2 89.0 89.8 90.3	(89.1)
3 90.0 88.8 90.0 88.7	88.4
4 91.6 89.4 90.0 90.2	89.8
5 90.4 89.6 89.8 90.2	88.4
6 90.4 88.4 90.0 90.0	88.4
7 92.3 90.2 93.0 91.8	92.4
8 91.8 90.4 93.1 91.5	90.4
9 91.8 89.6 92.4 91.2	90.2
10 92.2 91.0 93.2 92.4	91.8
11 91.8 91.0 93.2 92.7	92.4
12 92.5 91.2 93.5 92.6	92.2
13 92.2 91.2 93.7 93.1	91.6
14 92.2 91.0 93.7 93.0	94.2
15 93.0 91.4 93.8 93.8	93.4
16 93.4 91.4 94.2 93.6	92.0
17 93.8 91.4 94.2 (93.7)	(93.4)
18 94.4 91.9 94.0 93.6	95.5
19 94.8 92.0 93.9 93.8	95.6
20 94.5 92.4 93.8 93.8	94.4

 $^{^{\}star}$ In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-2 (Continued)

Car Code:	IIF 243*	<u>KI 137</u>	LIA 238	LIA 238	M V250
Car Number:	31	10	21	22	16
Laboratory:	41	5	29	29	8
Fuel No.					
1	88.4	88.4	89.5	89.2	89.9
2	(88.3)	86.0	89.6	89.6	88.9
3	88.4	89.2	88.8	90.3	89.3
4	88.8	88.0	89.8	90.2	89.3
5	88.8	86.8	89.6	90.6	88.9
6	89.2	89.2	89.5	90.2	89.6
7	89.6	92.2	91.8	92.4	91.8
8	90.6	٧٤.2	91.9	92.2	91.3
9	88.7	91.3	91.6	91.6	91.1
10	92.5	92.8	92.0	93.0	91.6
11	90.4	92.5	92.2	92.8	91.2
12	91.5	93.2	93.4	93.2	92.4
13	92.2	93.5	93.1	93.0	91.8
14	91.1	94.0	93.4	92.8	92.2
15	90.1	94.2	94.2	93.2	92.4
16	91.6	94.3	94.4	93.4	93.0
17	(91.7)	94.6	95.0	93.8	92.6
18	93.6	94.8	95.2	94.1	93.1
19	91.0	95.0	95.0	94.2	93.3
20	92.4	94.8	95.5	94.4	93.6

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-2 (Continued)

Car Code:	NC5 225	NC7 228	NFH 450	NH 450	NIG 230*
Car Number:	5	20	15	14	28
Laboratory:	4	26	8	8	35
Fuel No.					
1	89.0	87.6	89.2	89.8	88.8
2	89.4	88.6	89.4	89.2	88.9
3	88.4	86.8	89.1	89.1	88.4
4	89.9	89.0	89.6	90.2	89.2
5	89.4	88.4	89.6	90.3	88.9
6	0.88	86.6	88.8	88.8	88.8
7	90.0	91.0	91.4	92.3	90.9
8	90.0	89.2	91.4	92.4	91.4
9	90.0	89.1	90.6	92.0	90.6
10	90.0	90.0	91.4	92.4	91.4
11	91.4	91.4	91.6	92.4	91.6
12	91.2	91.4	92.2	92.8	92.5
13	91.6	90.8	92.2	92.9	91.8
14	91.0	90.8	91.8	92.6	92.3
15	90.6	90.2	91.8	93.0	92.2
16	91.1	90.4	92.2	93.4	92.8
17	92.4	90.6	92.6	93.4	(92.9)
18	92.3	92.6	92.7	93.4	93.0
19	92.4	91.7	92.8	93.6	93.2
20	91.2	93.6	93.0	93.5	93.2

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-2 (Continued)

Car Code:	NIJ 244	NIK 238	NIK 238	NL9 216*	0 V250
Car Number:	12	7	9	35 ·	1
Laboratory:	8	4	5 .	7	3
Fuel No.					
1	89.4	89.2	89.6	90.2	89.6
2	89.2	89.5	89.6	(90.1)	90.0
3	89.4	90.3	89.6	89.8	90.0
4	89.6	90.3	90.5	90.4	90.2
5	89.7	89.6	89.6	90.4	90.2
6	88.4	89.8	90.2	90.8	89.9
7	91.2	91.9	92.2	(91.6)	92.2
8	91.0	92.1	92.6	91.6	92.6
9	90.8	91.2	91.8	91.6	91.8
10	91.7	92.1	92.6	91.6	92.8
11	91.8	92.1	92.2	92.4	92.8
12	92.4	93.0	93.0	92.6	93.7
13	92.0	92.8	93.2	92.2	93.2
14	92.0	92.2	93.2	93.6	93.0
15	92.4	92.8	93.6	93.2	93.5
16	92.4	93.4	94.0	93.0	93.7
17	92.7	93.4	93.6	(93.5)	93.7
18	92.6	93.6	94.0	93.6	94.1
19	92.8	94.0	94.6	93.9	94.7
20	93.2	94.0	94.6	93.9	94.2

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-2 (Continued)

Car Code:	0 V250*	OCA 133	OCA 133	OCA 223	OCA 242
Car Number:	34	23	24	17	8
Laboratory:	7	29	29	26	4
Fuel No.					
1	92.2	88.9	88.3	88.7	88.8
2	(92.3)	89.0	88.2	89.8	88.8
3	91.4	89.7	89.0	88.8	89.6
4	93.5	89.8	89.1	90.0	90.0
5	92.2	89.8	89.9	89.0	89.6
6	93.5	89.4	89.6	88.2	89.6
7	(94.6)	91.1	91.4	91.5	93.0
8	95.6	91.0	90.8	90.8	92.4
9	94.6	89.5	90.8	91.3	91.2
10	95.2	90.6	91.8	92.4	93.0
11	95.2	91.6	92.0	92.2	93.0
12	96.0	92.6	92.6	92.4	93.2
13	95.4	92.6	92.8	91.9	93.4
14	95.3	92.6	92.3	92.2	93.0
15	95.8	93.1	92.8	93.2	94.4
16	97.2	93.2	92.7	93.0	94.4
17	(96.7)	93.4	92.8	93.4	93.9
18	96.8	93.5	92.9	93.0	93.9
19	96.7	93.6	92.9	94.2	94.6
20	96.7	94.0	93.2	94.2	95.0

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-2 (Continued)

AVERAGE FULL-THROTTLE ROAD OCTANE NUMBER RATINGS

Individual Cars

Car Code:	OCA 242	01_V258	OL_223	0L_223*	PC 137*	PC 137
Car Number:	11	6	3	37	36	19
car number:		0	3	37	30	13
Laboratory:	5	4	3	7	7	26
Fuel No.						
1	89.6	89.6	89.6	89.7	90.3	89.0
2	88.8	89.4	89.3	(90.4)	(90.3)	88.5
3	90.4	90.2	89.6	92.0	90.4	89.4
4	90.4	89.8	89.8	91.2	90.5	89.0
5	90.0	89.6	89.3	90.2	89.9	89.0
6	90.0	89.2	89.0	92.0	92.3	88.8
7	93.4	91.0	91.2	(93.8)	(93.3)	92.2
8	93.6	90.8	91.3	93.8	92.6	91.8
9	92.6	90.4	91.8	93.0	91.8	92.0
10	93.1	92.3	92.8	94.2	93.6	91.8
11	93.1	91.8	93.2	92.7	93.4	92.0
12	93.1	92.7	93.2	94.3	93.2	91.8
13	93.8	92.0	92.5	93.8	92.3	91.8
14	93.5	92.3	92.5	93.2	94.5	92.2
15	94.5	92.1	93.7	95.6	94.1	93.2
16	94.5	92.7	94.2	95.8	94.2	91.9
17	95.0	92.5	94.4	(95.4)	(95.3)	92.8
18	94.8	92.7	94.9	95.2	95.4	93.4
19	95.0	92.9	95.2	95.8	96.0	93.1
20	95.0	92.9	95.1	95.1	96.0	93.2

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-2 (Continued)

AVERAGE FULL-THROTTLE ROAD OCTANE NUMBER RATINGS

Car Code:	PC 137	PC 137	PL 217M*	E 215	T 218M*	T 222*
Car Number:	25	26	32	33	29	18
Laboratory:	30	30	47	50	41	26
Fuel No.						
1	86.4	86.1	90.5	88.5	92.4	88.8
2	90.7	88.8	(89.5)	88.5	(91.6)	89.6
3	91.2	89.5	90.0	88.5	91.7	89.4
4	90.8	88.0	90.4	89.0	92.6	90.9
5	89.4	88.4	90.4	89.0	91.4	89.5
6	91.8	91.4	90.2	87.0	91.8	90.9
7	94.0	91.0	92.2	89.0	96.3	93.3
8	91.8	92.1	91.8	89.0	95.0	92.3
9	92.2	91.4	91.5	88.5	94.7	92.4
10	93.3	91.8	93.5	90.0	95.1	92.8
11	93.0	92.7	93.7	90.0	93.0	92.8
12	93.1	92.2	93.8	91.5	95.2	93.5
13	94.0	92.0	93.5	91.5	93.4	93.1
14	93.4	94.2	94.0	89.5	95.7	95.2
15	94.2	94.2	93.4	89.5	95.6	(93.7)
16	95.4	93.7	93.4	90.5	94.7	93.9
17	95.8	95.8	94.0	90.5	(96.4)	94.6
18	95.5	94.2	94.0	91.5	97.8	94.9
19	95.9	95.6	94.6	91.5	97.4	95.6
20	96.4	95.6	94.8	91.5	97.0	95.4

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-3

AVERAGE PART-THROTTLE ROAD OCTANE NUMBER RATINGS

Individual Cars

Car Code:	LIA 238	LIA 238	NC5 225	NL9 216*	<u>0 V250</u> *	OCA 133
Car Number:	21	22	5	35	34	23
Laboratory:	29	29	4	7	7	29
Fuel No.						
1	87.0	86.0	83.4	81.8	87.3	87.2
2	87.6	86.7	83.8	(82.6)	(87.6)	87.4
3	87.0	86.1	83.4	82.6	87.0	87.4 87.2
4	87.6	86.8	84.2	83.4	87.8	87.4
5	87.0	87.4	83.8	83.2	88.4	
6	87.4	86.4	84.6	83.2		87.6
7	88.6	86.8	85.0	(83.3)	87.0	86.8
8	88.6	86.4		•	(88.6)	88.0
9	88.7		85.0	83.4	89.3	88.0
		86.5	84.1	82.3	88.2	87.8
10	88.6	87.3	86.0	83.8	90.4	89.1
11	89.4	88.7	85.4	83.8	89.4	89.4
12	90.2	89.0	85.9	84.4	91.0	89.8
13	90.2	87.8	85.7	84.2	90.4	89.5
14	89.8	88.4	85.8	85.6	8° 9	89.4
15	90.5	88.9	86.1	84.6	89.0	89.0
16	90.6	88.4	85.8	83.7	91.4	90.2
17	90.4	89.0	86.4	(84.8)	(90.8)	
18	91.2	88.2	86.7	•		89.8
19	91.8			85.0	90.4	90.6
		88.6	86.6	85.6	91.0	91.0
20	92.1	89.0	86.8	84.8	91.7	90.8

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

TABLE E-3 (Continued,

AVERAGE PART-THROTTLE ROAD OCTANE NUMBER RATINGS

'ndividual Cars

Car Code:	OCA 133	OCA 242	OCA 242	<u>01 V258</u>	<u>0L 223</u> *	PC 137*
Car Number:	24	8	11	6	37	36
Laboratory:	29	4	5	4	7	7
Fuel No.						
1	88.3	83.0	88.2	85.8	88.0	86.3
2	88.2	83.4	87.8	86.2	(88.3)	(86.6)
3	88.1	83.7	88.2	86.2	87.4	86.6
4	88.6	85.4	88.2	86.6	89.4	87.4
5	89.0	84.0	88.7	86.4	89.0	87.0
6	88.8	84.2	88.88	86.8	88.4	87.0
7	90.8	84.5	89.8	87.6	(89.4)	(87.9)
8	90.6	84.7	90.5	87.4	89.8	87.8
9	89.8	83.7	88.8	87.1	88.9	87.2
10	91.4	85.4	90.3	88.2	90.5	88.8
11	91.2	85.4	90.5	88.0	91.0	88.6
12	92.4	86.2	90.8	88.7	91.0	89.4
13	91.9	85.9	90.8	88.4	90.0	89.2
14	91.4	87.0	90.6	88.0	91.2	89.2
15	92.0	85.4	90.2	89.0	91.0	89.2
16	92.2	85.6	90.2	88.2	91.4	89.2
17	92.2	85.9	91.6	89.4	(91.8)	(89.7)
18	92.2	86.8	91.8	89.6	91.7	89.8
19	93.0	87.8	91.8	89.6	92.4	89.8
20	92.9	87.8	91.6	90.0	93.6	90.4

^{*} In developing the averages, it was necessary to estimate some ratings. Numbers in () contain such estimated ratings.

APPENDIX F

MULTIPLE REGRESSION EQUATIONS

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MULTIPLE REGRESSION EQUATIONS

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TABLE F-1

1.30

FULL-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; 37 Cars; Road ON Mean = 91.900

	(R+M)/2 b ₅							0.690	
	R×M b ₈								
	(MON) ² b ₇								
ents*	(RON) ² b ₆								-0.020 (0.0020)
Coefficients*	Ethanol b ₄					$\frac{0.015}{(0.3\sqrt{2})}$	0.014 (0.323)		
	Heavy Aromatics b ₃				-0.009		<u>-0.009</u> (0.212)		
	WON P2		0.840	0.450	0.457	0.430	0.437		0.425
	RON b ₁	0.490		0.286	0.284	0.300	0.295		3.997
	Constant* b ₀	45.578 (0.0001)	19.870 (0.0094)	26.275 (0.0001)	26.005 (0.0001)	26.599 (0.0001)	26.616 (0.0001)	29.700 (0.0001)	0.988 -143.663 (0.0065)
	R2	0.882	0.861	0.977	0.979	0.979	0.981	0.972	. 988
	Std.	0.608	0.659	0.276	0.269	0.275	0.269	0.296	0.209
	Eqn.	_	8	ო	4	က	9	7	ထ

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR \geqslant 0.05) are underlined.

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TABLE F-1 (Continued)

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FULL-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; 37 Cars; Road ON Mean # 91.900

	(R+M)/2 b ₅								
	RxM b ₈								-0.032 (0.559)
	(MON) ²	-0.001 (0.974)			0.000	-0.001 (0.963)		0.000)	-0.015 (0.785)
ents*	(RON) ² b ₆		-0.021 (0.0003)	-0.019 (0.0023)			-0.021 (0.0004)		-0.031 (0.091)
Coefficients*	Ethanol b ₄			$\frac{0.013}{(0.240)}$		0.015	$\frac{0.012}{(0.220)}$	0.014	
	Heavy Aromatics b ₃		-0.012 (0.019)		<u>-0.009</u> (0.209)		-0.011 (0.021)	<u>-0.009</u> (0.229)	
	MON b2	0.564 (0.872)	0.432 (0.0001)	0.408	0.422 (0.902)	$\frac{0.593}{(0.865)}$	0.416 (0.0001)	$\frac{0.455}{(0.894)}$	-0.093
	RON b ₁	0.286	4.294 (0.0002)	3.942 (0.0012)	0.284	0.298	4.236 (0.0002)	0.295	$\frac{3.329}{(0.110)}$
	Constant* b ₀	23.853	-163.216 (0.0012)	-146.002 (0.0075)	29.006	20,164 (0,894)	-156.431 (0.0014)	$\frac{25.073}{(0.860)}$	-86.898 (0.505)
	R ²	0.997	0.991	0.989	0.979	0.979	0.992	0.981	0.989
	Std. Dev.	0.284	0.178	0.206	0.278	0.284	0.175	0.278	0.213
	Egn.	Ø	10	:	12	13	4	15	16

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-2

FULL-THROTTLE RUAD ON REGRESSION EQUATIONS

All-Car Averages; Cars That Tested All Fuels; 26 Cars; Road ON Mean = 91.620

•						Coeffic	ients*		•
Egn.	Std. Dev.	R ²	Constant* bo	RON	MON b ₂	Heavy Aromatics Ethau	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
-	0.599	0.886	45.109 (0.0001)	0.492					
~	0.673	0.856	19.590 (0.012)		0.840 (0.0001)				
ო	0.279	0.977	26.105 (0.0001)	0.293	0.441				
4	0.276	0.978	25.905 (0.0001)	0.291	0.447	$\frac{-0.008}{(0.268)}$			
ഗ	0.282	0.978	26.486 (0.0001)	0.302	0.426 (0.0001)		0.012 (0.435)		
.,	0.280	0.979	26.290 (0.0001)	0.300	0.432 (0.0001)	$\frac{-0.008}{(0.292)}$	$0.011 \\ (0.466)$		
α	0.196	0.989	-166.583 (0.0019)	4.341 (0.0003)	0.414 (0.0001)			-0.021 (0.0006)	
01	0.169	0.992	-174.765 (0.0004)	4.613 (0.0001)	0.420	-0.011 (0.022)		-0.023 (0.0001)	

* Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

TABLE F-3

Carried Carry

FULL-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; Automatic Transmissions; 35 Cars; Road ON Mean 🤊 🐠 🧺

	(MON) ² b ₇								
	(RON) ² b ₆							-0.020 (0.0008)	-0.021 (0.0002)
ients*	Ethanol b4					$\frac{0.015}{(0.278)}$	$\frac{0.014}{(0.302)}$		
Coefficients*	Heavy Aromatics b ₃				$\frac{-0.007}{(0.311)}$		-0.006 (0.336)		-0.009
	MON b ₂		0.841	0.453	0.458 (0.0001)	0.433	0.438	0.428 (0.0001)	0.433
	RON b ₁	0.490		0.285	0.284 (0.0001)	0.297 (0.0001)	0.295	3.993 (0.0004)	4.229 (0.3001)
	Constant*	45.478 (0.0001)	19.684 (0.0093)	26.013 (0.0001)	25.788 (0.0001)	26.525 (0.0001)	26.384 (0.0001)	-143.642 (0.0028)	-157.303 (0.0007)
	R ²	0.883	0.864	0.980	0.981	0.981	0.982	066.0	0.993
	Std. Dev.	0.603	0.651	0.259	0.255	0.257	0.257	0.185	0.165
	Egn.	-	2	က	4	ro ,	9	ω	10

* Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

TABLE F-4

FULL-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; U.S. Cars; 34 Cars; Road ON Mean = 91.865

						Coefficients*	ients*		
Egn.	Std.	R ²	Constant*	RON b ₁	MON b ₂	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
_	0.615	0.879	45.637 (0.0001)	0.489					
7	0.654	0.863	19.664 (0.0096)		0.842 (0.0001)				
ო	0.278	0.977	25.924 (0.0001)	0.283	0.457				
4	0.274	0.989	25.723 (0.0001)	0.281	0.463	-0.008 (0.232)			
വ	0.279	0.978	26.463 (0.0001)	0.293 (0.0001)	0.439 (0.0001)		$(\frac{0.013}{0.370})$		
9	0.276	0.980	26.181 (0.0001)	0.291 (0.0001)	0.446	-0.008 (0.254)	$\frac{0.012}{(0.397)}$		
∞	0.202	0.988	-163.223 (0.0033)	4.199 (0.0005)	0.430 (0.0001)			-0.020 (0.0010)	
10	0.173	0.992	-172.540 (0.0006)	4.483 (0.0001)	0.436	-0.011 (0.020)		-0.022 (0.0002)	

* Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

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TABLE F-5

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FULL-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; Imported Cars; 3 Cars; Road ON Mean = 92.255

						COETTIC	1ents*		
Egn.	Std. Dev.	R ²	Construt*	RON b ₁	MON b ₂	Heavy Aromatics Etha	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
	0.770	608.0	48.013 (0.0001)	0.468					
7	0.726	0.830	21.683 (0.010)		0.823				
ო	0.516	0.919	27.204 (0.0001)	0.250 (0.0005)	0.483				
4	0.482	0.934	26.648 (0.0001)	0.245 (0.0003)	0.499	-0.022 (0.080)			
က	0.508	0.926	28.562 (0.0001)	0.274 (0.0003)	0.439		0.032 (0.234)		
9	0.474	0.940	27.853 (0.0001)	0.268 (0.0003)	0.458	$\frac{-0.022}{(0.087)}$	$(0.030 \ (0.238)$		

* Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

TABLE F-6

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FULL-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; PC 137; 4 Cars; Road ON Mean = 92.290

						Coefficients*	ients*		
Eqn.	Std. Dev.	R ²	Constant* b ₀	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
-	0.853	0.847	36.325 (0.0001)	0.592 (0.0001)					
2	0.959	908.0	6.283 (0.534)		1.003 (0.0001)				
က	0.604	0.927	14.345 (0.040)	0.361	0.511 (0.0004)				
4	9.618	0.928	14.475 (0.043)	0.363 (0.0001)	0.506 (0.0007)	$\frac{0.007}{(0.645)}$			
S	0.440	0.964	17.954 (0.0017)	0.430	0.388 (0.0006)		0.091		
9	0.443	996.0	,8.306 (0.0018)	0.432 (0.0001)	0.380	$\frac{0.009}{(0.402)}$	0.092 (0.0011)		

* Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

TABLE F-7

FULL-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; 0 V250/M V250; 3 Cars; Road ON Mean = 92.820

						Coafficients*	ients*		
Eqn.	Std.	R ²	Constant*	RON P ₁	MON b ₂	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
	0.579	0.881	196 00	0.465					
2	0.707	0.823	25.349 (0.0024)		0.781				
ო	0.358	0.957	32.365 (0.00U1)	0.293 (0.0001)	0.382				
4	0.365	0.958	32.194 (0.0001)	0.292 (0.0001)	0.386	$\frac{-0.005}{(0.557)}$			
ιΩ	0.366	0.958	32.700 (0.0001)	0.299	0.371 (0.0002)		0.009 (0.648)		
9	0.374	0.959	32.534 (0.0001)	0.298	0.375 (0.0002)	$\frac{-0.005}{(0.53)}$	0.008 (0.676)		
œ	908.0	0.971	153.036 (0.041)	4,263 (0.011)	0.356 (0.0001)			-0.021 (0.016)	

* Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

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TABLE F-8

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 3; Car No. 2; 20 Fuels; Road ON Mean = 92.135

							Coefficients*	nts*		
Car Code	Eqn.	Std. Dev.	R ²	Constant* bo	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
HC5 225	-	0.658	0.829	51.769 (0.0001)	0.472 (0.0001)					
	2	0.684	0.815	29.023 (0.0007)		0.736 (0.0001)				
	က	0.458	0.921	34.485 (0.0001)	0.247 (0.0C32)	0.400				
	4	0.454	0.928	34.213 (0.0001)	0.244 (0.0002)	0.409 (0.0003)	-0.013 (0.?66)			
	S	0.393	0.946	36.708 (0.0001)	0.288	0.326 (0.0010)		0.054 (0.017)		
	9	0.387	0.951	36.433 (0.0001)	0.284 (0.0001)	0.336	$\frac{-0.012}{(0.244)}$	0.053 (0.018)		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

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(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 8; Car No. 13; 20 Fuels; Road ON Mean = 90.515

	(MON) ²						
	(RON) ² b ₆						
nts*	Ethanol b4					$\frac{-0.025}{(0.156)}$	$\frac{-0.026}{(0.109)}$
Coefficients*	Heavy Aromatics b ₃				$\frac{-0.014}{(0.102)}$		$\frac{-0.014}{(0.074)}$
	MON		0.580	0.378 (C.0001)	0.388 (0.0001)	0.411 (0.0001)	0.424 (0.0001)
	RON	0.319		0.148	0.145	0.130	3.126 (0.0029)
	Constant*	60.358	40.780 (0 0001)	44.110 (0.0001)	43.769 (0.0001)	43.096 (0.0001)	42.597 (0.0001)
	R ²	0.788	0.864	0.930	0.941	0.938	0.950
	Std.	0.560	0.449	0,333	0.315	0.321	0.297
	Egn.		2	ო	4	ro	9
	Car Code	HIA 238					

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 3; Car No. 4; 20 Fuels; Road ON Mean = 92.455

					Coefficients* Heavy	nts*	c	c
Std. Constant* Eqn. Dev. R ² b ₀	Constant* b ₀	Ì	RON b ₁	MON b2	Aromatics b ₃	Ethanol b4	(RON)	(MON) ²
0.719 0.843 45.944 0 (0.0001) (0		00	0.492 (0.0001)					
0.975 0.712 25.055 (0.023)	25.055 (0.023)			0.786				
0.640 0.883 33.067 0. (0.0002) (0.			0.357	0.299 (0.028)				
0.659 0.883 32.998 0. (0.0002) (0.		0.00	0.357	0.300	$\frac{-0.001}{(0.926)}$			
0.659 0.883 33.126 0.3 (0.0003) (0.0		0.0	0.359 (0.0003)	0.296 (0.045)		$\frac{0.002}{(0.943)}$		
0.680 0.883 33.057 0.3 (0.0005) (0.00		(0.0	0.359	0.297 (0.053)	$\frac{-0.001}{(0.931)}$	$\frac{0.002}{(0.948)}$		
0.398 0.957 -443.764 10.4 (0.0002) (0.0	43.764 (0.0002)	10.4	10.473	0.231			-0.053 (0.0001)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 35; Car No. 27; 19 Fuels (Except 17); Road ON Mean = 91.921

							Coefficients*	ints*		
Car Code	Egn.	Std. Dev.	R2	Constant* b ₀	RON	RON S	Heavy Aromatics b ₃	Ethanol b4	(RON) ² _{b6}	(MON) ² b ₇
HIK 238	-	0.745	0.796	50.691 (0.0001)	0.437					
	2	0.670	0.820	26.144 (0.0027)		0.768 (0.0001)				
	т	0.500	0.914	30.780 (0.0001)	0.235 (0.0007)	0.455 (0.0003)				
	4	0.487	0.923	30.746 (0.0001)	0.229 (0.0008)	0.465	$\frac{-0.017}{(0.192)}$			
	ς.	0.516	0.914	30.934 (0.0001)	0.236 (0.0017)	0.452 (0.0007)		$\frac{0.002}{(0.931)}$		
	9	0.504	0.923	30.759 (0.0001)	0.228 (0.0021)	0.466 (0.0005)	$\frac{-0.017}{(0.209)}$	$\frac{-0.001}{(0.978)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS Lab 41; Car No. 30; 18 Fuels (Except 2, 17); Road ON Mean = 91.678

							Coefficients*	nts*		
Car Code	Egn.	Std. Dev.	R2	Constant* b ₀	RON	MON b ₂	Heavy Aromatics b ₃	Ethanol b4	$(RON)^2$ b_6	(MON) ² b ₇
HLV 225	-	1,353	069.0	32.536 (0.0048)	0.625 (0.0001)					
	2	1.203	0.755	$\frac{-2.414}{(0.858)}$		1.097				
	က	1.035	0.830	$\frac{1.445}{(0.901)}$	0.310 (0.021)	0.710 (0.0031)				
	4	0.818	0.901	$\frac{3.133}{(0.739)}$	0.268 (0.015)	0.749	-0.068 (0.0069)			
	S	0.992	0.854	$\frac{4.339}{(0.698)}$	0.368 (0.0091)	0.606		$\frac{0.079}{(0.150)}$		
	9	0.765	0.919	$\frac{5.678}{(0.524)}$	0.321 (0.0049)	0.657 (0.0012)	-0.066 (0.0063)	0.070		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

TABLE F-8 (Continued)

FULL-THRUTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 41; Car No. 31; 18 Fuels (Except 2, 17); Road ON Mean = 90.494

Constant* RON		MON	Coefficients* Heavy Aromatics Eth	nts* Ethanol	(RON) ² b ₆
1	-			-	
0.538 55.009 0. (0.0001) (0.	0.375				
0.689 29.510 (0.011)		0.711			
0.719 31.180 0. (0.0078) (0.0	0.131	0.547			
0.689 30.414 (0.014)		0.701	$\frac{-0.003}{(0.915)}$		
0.795 26.447 (0.0081)		0.752 (0.0001)		-0.106 (0.014)	
0.796 26.514 (0.010)		0.752	-0.004 (0.850)	-0.107 (0.017)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 5; Car No. 10; 20 Fuels; Road ON Mean = 91.850

					Coefficients*	nts*		
Std. Dev.	R ²	Constant*	RON	MON b ₂	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
1.090	0.865	$\frac{14.993}{(0.051)}$	0.813					
1.534	0.732	$\frac{-19.539}{(0.235)}$		(0.0001)				
0.934	906.0	-6.440 (0.525)	0.588 (0.0001)	0.498				
0.962	0.906	$\frac{-6.413}{(0.543)}$	0.589	0.496 (0.018)	$(\frac{0.003}{0.892})$			
0.959	0.906	-5.761 (0.585)	0.600	0.476 (0.029)		(0.016)		
0.990	0.907	-5.669 (0.604)	0.601	0.473 (0.036)	$\frac{0.004}{(0.883)}$	(0.017)		
0.634	0.959	-655.626 (0.0003)	14.536 (0.0002)	0.404			-0.074 (0.0003)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 29; Car No. 21; 20 Fuels; Road ON Mean = 92.275

							Coefficie	ints*		
Car Code	Egn.	Std.	R ²	Constant*	RON b ₁	MON b2	Heavy Aromatics Etl b ₃	Ethanol b4	(RON) ² be	(MON) ² b ₇
LIA 238	-	0.804	0.876	32.623 (0.0001)	0.631					
	8	0.857	0.859	-0.850 (0.923)		1.086 (0.0001)				
	က	0.387	0.973	$\frac{7.340}{(0.095)}$	0.366 (0.0001)	0.587				
	4	0.396	0.973	(0.109)	0.365	0.590	$\frac{-0.004}{(0.659)}$			
	ည	0.394	0.974	(0.088)	0.376	0.571		$\frac{0.012}{(0.554)}$		
	ဖ	0.405	0.974	$(\frac{7.715}{0.103})$	0.374 (0.0001)	0.574 (0.0001)	-0.004 (0.688)	$\frac{0.011}{(0.579)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 29; Car No. 22; 20 Fuels; Road ON Mean = 92.210

							Coefficients*	nts*		
Car Code	Eqn.	Std. Dev.	R2	Constant*	RON	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ²
LIA 238		0.627	0.860	48.724 (0.0001)	0.460					
	2	0.650	0.850	24.125 (0.0021)		0.794 (0.0001)				
	ო	0.351	0.959	30.046 (0.0001)	0.263	0.435				
	4	0.360	0.959	29.924 (0.0001)	0.263 (0.0001)	0.437 (0.0001)	-0.003 (0.731)			
	æ	0.351	0.959	30.019 (0.0001)	0.265 (0.0001)	0.433		$\frac{0.002}{(0.924)}$		
	ω	0.372	0.959	29.997 (0.0001)	0.264 (0.0001)	0.435	$\frac{-0.003}{(0.743)}$	$\frac{0.001}{(0.940)}$		
	ထ	0.209	0.986	-235.076 (0.0001)	5.938 (0.0001)	0.397 (0.0001)			-0.030	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 8; Car No. 16; 20 Fuels; Road ON Mean = 91.365

							Coefficients*	nts*		
Car Code	Eqn.	Std. Dev.	R ²	Constant* b ₀	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
M V250	٦	0.541	0.884	49.770 (0.0001)	0.440					
	8	0.765	0.767	30.311 (0.0012)		0.712 (0.0001)				
	ო	0.420	0.934	37.123 (0.0001)	0.308	0.293 (0.0023)				
	4	0.428	0.935	36.984 (0.0001)	0.306 (0.0001)	0.298 (0.0026)	-0.006 (0.559)			
	വ	0.426	0.936	37.717 (0.0001)	0.320 (0.0001)	0.272 (0.0071)		$\frac{0.016}{(0.479)}$		
	9	0.435	0.937	37,582 (0.0001)	0.318 (0.0001)	0.277 (0.0079)	-0.00 6 (0.590)	$\frac{0.015}{0.508}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence levei (PR>0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 4; Car No. 5; 20 Fuels; Road ON Mean = 90.465

							Coefficients*	ints*		
Car Code	Egn.	Std. Dev.	R ²	Constant*	RON b ₁	MON b ₂	Heavy Aromatics b ₃	Ethanol b4	(RON) ² _{b6}	(MON) ² b ₇
NC5 225		0.833	0.594	62.388 (0.0001)	0.297					
	2	0.627	0.770	40.044 (0.0001)		0.588				
	m	0.619	0.789	41.887 (0.0001)	$\frac{0.083}{(0.249)}$	0.475				
	4b	0.605	0.798	39.655 (0.0001)		0.597 (0.0001)	$\frac{-0.023}{(0.147)}$			
	2 p	0.642	0.772	39.760 (0.0001)		0.592 (0.0001)		$\frac{-0.013}{(0.693)}$		
	q9	0.620	0.800	39.290 (0.0001)		0.602 (0.0001)	$\frac{-0.023}{(0.154)}$	$\frac{-0.014}{(0.648)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

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TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 26; Car No. 20; 20 Fuels; Road ON Mean = 89.990

							Coefficients*	ints*		
Car Code	Eqn.	Std. Dev.	R ²	Constant* bo	RON b1	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ²	$(MON)^2$
NC7 228	~	1.244	0.564	50.474 (0.0001)	0.418					
	2	0.912	0.766	$\frac{17.531}{(0.080)}$		0.845				
	ო	0.916	0.777	19.621	$\frac{0.094}{(0.373)}$	0.717 (0.0009)				
	4 b	0.820	0.821	16.667 (0.067)		0.864 (0.0001)	-0.046 (0.035)			
	2 p	0.934	0.768	17.959 (0.082)		0.839 (0.0001)		$\frac{0.019}{(0.680)}$		
	9	0.841	0.823	17.022 (0.071)		0.859 (0.0001)	-0.046	0.016 (0.699)		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 8; Car No. 15; 20 Fuels; Road ON Mean = 91.170

							Coefficients*	nts*		
Car Code	Egn.	Std. Dev.	R ²	Constant*	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
NFH 450		0.617	0.814	55.152 (0.0001)	0.381					
	2	0.569	0.842	33.460 (0.0001)		0.673 (0.0001)				
	ო	0.394	0.929	37.868 (0.0001)	0.201	0.400				
	4	0.397	0.931	37.676 (0.0001)	0.199	0.406	-0.008 (0.419)			
	ഗ	0.404	0.929	37.610 (0.0001)	0.195	0.410		$\frac{-0.007}{(0.741)}$		
	Q	0.408	0.932	37.336 (0.0001)	0.193 (0.0012)	0.417	$\frac{-0.008}{(0.422)}$	-0.008 (0.713)		
	æ	0.332	0.952	-170.576 (0.035)	4.702 (0.0095)	0.370			-0.024 (0.012)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 8; Car No. 14; 20 Fuels; Road ON Mean = 91.875

							Coefficients*	nts*		
Car Code	Ean.	Std. Dev.	22	Constant* b ₀	RON b ₁	MON b ₂	Heavy Aromatics b ₃	Ethanol b ₄	$(RON)^2$	$(MON)^2$
NH 450	~	0.685	0.835	48.862 (0.0001)	0.455					
	7	0.873	0.732	28.420 (0.0056)	•	0.740				
	ო	0.588	0.885	35.351 (0.0001)	0.314 (0.0002)	0.313				
	4	0.602	0.887	35.228 (0.0001)	0.312 (0.0003)	0.318 (0.016)	<u>-0.007</u> (0.655)			
	ហ	909.0	0.885	35.224 (0.0001)	0.311	0.318 (0.022)		$\frac{-0.004}{(0.903)}$		
	9	0.621	0.887	35.020 (0.0001)	0.309 (0.0008)	0.324 (0.024)	-0.007 (0.660)	-0.00 5 (0.888)		
	ω	0.467	0.932	-314.124 (0.0092)	7.743	0.263 (0.012)			-0.039 (0.0045)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 35; Car No. 28; 19 Fuels (Except 17); Road ON Mean = 91.047

							Coefficients*	ints*		
Car Code	Eqn.	Std. Dev.	R ²	Constant*	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(mon) ² b ₇
NIG 230	-	0.718	0.832	46.326 (0.0001)	0.474 (0.0001)					
	2	0.684	0.848	20.045 (0.014)		0.829 (0.0001)				
	ო	0.406	0.949	25.149 (0.0001)	0.260 (0.0001)	0.483				
	4	0.411	0.951	25.210 (0.0001)	0.257 (0.0001)	0.487	$\frac{-0.008}{(0.444)}$			
	ស	0.419	0.949	25.222 (0.0001)	0.261	0.481		0.001		
	ဖ	0.426	0.951	25.125 (0.0001)	0.257 (0.0002)	0.488	$\frac{-0.008}{(0.4^{4})}$	(0.000)		
	∞	0.366	0.962	-157.850 (0.0813)	4.112 (0.035)	0.455			-0.020 (0.046)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 8; Car No. 12; 20 Fuels; Road ON Mean = 91.235

							Coefficie	nts*		
Car Code	Egn.	Std. Dev.	R ²	Constant*	RON b ₁	MON b2	Heavy Aromatics Ethai b ₃ b ₄	Ethanol b4	(RON) ² b ₆	(MON) ²
NIJ 244	_	0.621	0.828	53.232 (0.0001)	0.402					
	2	0.652	0.810	32.067 (0.0002)		0.690				
	က	0.440	0.918	37.301 (0.0001)	0.234 (0.0002)	0.371				
	4	0.434	0.925	36.943 (0.0001)	0.231	0.381 (0.0004)	-0.013 (0.242)			
	ហ	0.447	0.921	36.621 (0.0001)	0.222 (0.0007)	0.393		$\frac{-0.016}{(0.509)}$		
	9	0.440	0.928	36.277 (0.0001)	0.218 (0.0008)	0.404	<u>-0.013</u> (0.236)	-0.017 (0.465)		
	æ	0.396	0.938	$\frac{-165.839}{(0.089)}$	4.488 (0.032)	0.343			-0.022 (0.040)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 4; Car No. 7; 20 Fuels; Road ON Mean = 91.865

							Coefficients*	ints*		
Car Code	Egn	Std. Dev.	R ²	Cons tant*	RON b ₁	MON h2	Heavy Aromatics b ₃	Ethanol bą	(RON) ² b ₆	(MON) ²
NIK 238	~	0.570	0.877	49.419 (0.0001)	0.449					
	8	0.658	0.836	26.523 (0.0011)		0.762 (0.0001)				
	က	0.329	0.961	32.614 (0.0001)	0.273 (0.0001)	0.39 0 (0.000)				
	4	0.338	0.962	32.424 (0.0001)	0.273	0.393	-0.004 (0.679)			
	ιΩ	0.339	0.961	32.606 (0.0001)	0.274 (0.0001)	0.389		$\frac{0.000}{(0.978)}$		
	ဖ	0.349	0.962	32.509 (0.0001)	0.273	0.392 (0.0001)	<u>-0.004</u> (0.690)	0.000		
	x c	0.271	0.975	-149.486 (0.025)	4.209 (6.0053)	0.363			-0.021 (0.0082)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CAKS

Lab 5; Car No. 9; 20 Fuels; Road ON Mean = 92.215

							Coefficients*	nts*		
Car Sode	Eqn.	Std. Dev.	R ²	Constant*	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² be	(MON) ² b ₇
NIK 238	-	0,625	0.881	44.853 (0.0001)	0.501					
	8	0.738	0.834	19.585 (0.020)		0.847				
	(C)	0.362	0,962	26.388 (0.0001)	0.309	0.427				
	4	0.372	0.962	26.430 (0.0001)	0.308	0.428	-0.002 (0.852)			
	တ	0.362	0.964	27.135 (0.0001)	0.322	0.403		$\frac{0.018}{(0.349)}$		
	9	6.374	0.964	27.066 (0.0001)	0.322	0.404	-0.001 (0.890)	(0.018)		
	ස	0.313	0.973	-153.159 (0.041)	4.218 (0.013)	0.400			-0.021	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

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(Continued)

Lab 7; Car No. 35; 17 Fuels (Except 2, 7, 17); Road ON Mean = 92.047 FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

							Coefficients*	nts*		
Car Code	Eqn.	Std. Dev.	R ²	Constant* bo	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
NL9 216	-	0.702	0.757	56.766 (0.0001)	0.373					
	8	0.534	0.859	34.366 (0.0001)		0.672 (0.0001)				
	က	0.409	0.923	37.110 (0.0001)	0.167	0.456				
	4	0.424	0.923	37.237 (0.0001)	0.166 (0.0062)	0.456 (0.0001)	-0.002 (0.850)			
	အ	0.371	0.941	39,490 (0.0001)	0.209	0.380		0.043		
	ø	0.385	0.942	39.633 (0.0001)	0.208 (0.0015)	0.380	-0.003 (0.796)	0.043		

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Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 3; Car No. 1; 20 Fuels; Road ON Mean = 92.295

							Coefficients*	nts*		
Car Code	Egn.	Std.	R ²	Constant*	RON	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RCW) ² b ₆	(MON) ² b ₇
0 V250	~	0.657	0.857	47.296 (0.0001)	0.476					
	~	0,699	0.839	22.237 (0.0066)		0.817				
	က	0.397	0.951	28.379 (0.0001)	0.277	0.440				
	4	0.390	0,955	28.176 (0.0001)	0.274 (0.0001)	0.448	$\frac{-0.012}{(0.219)}$			
	ហ	0.407	0.951	28.125 (0.0001)	0.271	0.450		(0.707)		
	9	0.400	0.956	27.780 (0.0001)	0.267	0.461	-0.013	-0.009 (0.656)		
-	ထ	0.304	0.973	-217.825 (0.0056)	5.561 (0.0016)	0.404			-0.028 (0.0023)	
	10	0.265	0.981	-230.185 (0.0013)	5.970 (0.0003)	0.413	-0.016 (0.028)		-0.031 (0.0005)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 7; Car No. 34; 17 Fuels (Except 2, 7, 17); Road ON Mean = 94.900

							Coefficients*	ints*		
Car Code	Egn.	Std. Dev.	R2	Constant*	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
0 V250	,	0.796	0.807	48.552 (0.0001)	0.490					
	20	0.882	0.764	25.717 (0.021)		0.806				
	ო	0.616	0.892	30.627 (0.0007)	0.302 (0.001)	0.416				
	4	0.639	0.892	30.627 (0.0011)	0.302 (0.0017)	0.416 (0.0069)	$\frac{0.000}{(0.978)}$			
	ഗ	0.623	0.898	32.228 (0.0008)	0.331	0.364 (0.023)		$\frac{0.030}{(0.421)}$		
	9	0.648	0.898	32.228 (0.0013)	0.331 (0.0023)	0.364 (0.029)	0.000)	$\frac{0.030}{(0.440)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 29; Car No. 23; 20 Fuels; Road ON Mean = 91.450

							Coefficients*	ints*		
Car Code	Eqn.	Std. Dev.	R ²	Constant* b ₀	RON b ₁	MON b ₂	Heavy Aromatics b ₃	hanol 54	(RON) ² b 6	(MON) ²
0CA 133	-	0.816	0.797	46.357 (0.0001)	0.477					
	2	0.604	0.889	16.419 (0.017)		0.875 (0.0001)				
	ო	0.417	0.950	21.150 (0.0002)	0.213 (0.0003)	0.585				
	4	0.430	0.950	21.219 (0.0003)	0.213 (0.0004)	0.584 (0.0001)	$\frac{0.001}{(0.922)}$			
	ည	0.409	0.955	20.172 (0.0003)	0.192	0.621 (0.0001)		$\frac{-0.027}{(0.220)}$		
	9	0.423	0.955	20.077 (0.0005)	0.193 (0.0016)	0.621 (0.0001)	0.000 (0.971)	$\frac{-0.027}{(0.237)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 29, Car No. 24; 20 Fuels; Road ON Mean = 91.295

							Coefficients*	nts*		
Car Code	Egn.	Std.	R ²	Constant*	RON b ₁	MON	Heavy Aromatics b ₃	Ethanol E4	(RON) ² b ₆	(MON) ² b ₇
0CA 133	-	0.750	0.816	47.242 (0.0001)	0.466					
	7	0.672	0.852	20.380 (0.0090)		0.827				
	က	0.455	0.936	25.732 (0.0001)	0.240 (0.0002)	0.500				
	4	0.466	0.937	25.880 (0.0001)	0.241 (0.0003)	0.496	$\frac{0.006}{(0.526)}$			
	ည	0.464	0.937	25.039 (0.0001)	0.229 (0.0007)	0.521		$\frac{-0.015}{(0.532)}$		
	9	0.475	0.938	25.295 (0.0002)	0.230 (0.0010)	0.516 (0.0001)	$\frac{0.005}{(0.655)}$	$\frac{-0.015}{(0.559)}$		
	ω	0.312	0.972	-287.937 (0.0008)	7.003 (0.0003)	0.454 (0.0001)			-0.036 (0.0004)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

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TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 26; Car No. 17; 20 Fuels; Road ON Mean = 91.510

	(MON) ² b ₇						
	(RON) ² b ₆						
nts*	Ethanol b4					0.046 (0.154)	(0.042)
Coefficients*	Heavy Aromatics b ₃				-0.031 (0.036)		-0.030 (0.036)
	MON b2		0.878 (0.0001)	0.469 (0.0010)	0.491 (0.0003)	0.408 (0.0041)	0.434 (0.0012)
	RON b ₁	0.512 (0.0001)		0.300	0.293 (0.0002)	0.334 (0.0002)	0.325 (0.0301)
	Constant*	43.108 (0.0001)	$\frac{16.222}{(0.087)}$	22.933 (0.0026)	22.223 (0.0016)	24.740 (0.0014)	23.878 (0.0008)
	R ²	0.817	0.797	0.905	0.928	0.916	0.938
	Std.	0.821	0.866	0.610	0.545	0.589	0.522
	Eqn.	, -	2	ო	4	ro	9
	Car Code	0CA 223					

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 4; Car No. 8; 20 Fuels; Road ON Mean = 92.240

							Coefficients*	ents*		
Car Code	Egn.	Std. Dev.	R ²	Constant* b ₀	RON b ₁	MON b ₂	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
OCA 242		0.705	0.893	35.519 (0.0001)	0.600					
	2	0.972	0.796	7.862 (0.444)		0.984 (0.0001)				
	ო	0.485	0.952	16.918 (0.0045)	0.404	0.433				
	4	0.492	0.953	16.648 (0.0059)	0.403	0.439	$\frac{-0.009}{(0.495)}$			
	ស	0.495	0.953	17.444 (0.0051)	0.415	0.414 (0.0009)		$\frac{0.014}{(0.598)}$		
	9	0.504	0.954	17.265 (0.0068)	0.412 (0.0001)	0.421	$\frac{-0.008}{(0.523)}$	$\frac{0.013}{(0.628)}$		
	ω	0.363	0.975	-292.160 (0.0025)	7.023 (0.0010)	0.388			-0.035 (0.0016)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

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TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 5; Car No. 11; 20 Fuels; Road ON Mean = 92.710

							Coefficients*	ents*		
Car Code	Egn.	Std. Dev.	R ²	Constant*	RON b1	MON b ₂	Heavy Aromatics b ₃	Ethanol b ₄	(RON) ² b ₆	(MON) ² b ₇
0CA 242	r	0.610	0.917	36.273 (0.0001)	0.597					
	7	1.110	0.724	13.648 (0.250)		0.922 (0.0001)				
	က	0.521	0.943	24.097 (0.0004)	0.470 (0.0001)	0.282 (0.013)				
	4	0.530	0.944	24.290 (0.0006)	0.472 (0.0001)	0.276 (0.017)	$\frac{0.008}{(0.541)}$			
	က	0.521	0.946	25.175 (0.0004)	0.490	0.246 (0.037)		$\frac{0.026}{(0.334)}$		
	9	0.530	0.948	25.419 (0.0005)	0.493	0.238	0.009 (0.509)	$\frac{0.028}{(0.237)}$		
	∞	0.281	0.984	-383.673 (0.0001)	9.281 (0.0001)	0.222 (0.0010)			-0.047 (0.0001)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

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TABLE F-8 (Continued)

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FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 4; Car No. 6; 20 Fuels; Road ON Mean = 91.345

							Coefficients*	ints*		
Car Code	Eqn.	Std. Dev.	R ²	Constant*	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ²
01 V258	-	0.640	0.785	57.312 (0.0001)	0.360					
	7	0.585	0.820	36.465 (0.0001)		0.640				
	က	0.449	0.900	40.576 (0.0001)	0.186 (0.0018)	0.387 (0.0004)				
	4	0.436	0.911	40.260 (0.0001)	0.182 (0.0018)	0.398 (0.0003)	$\frac{-0.015}{(0.174)}$			
	ស	0.430	0.913	39.258 (0.0001)	0.159 (0.0066)	0.434 (0.0002)		$\frac{-0.035}{(0.131)}$		
	9	0.410	0.926	38.805 (0.0001)	0.154 (0.0064)	0.448	$\frac{-0.016}{(0.131)}$	$\frac{-0.037}{(0.101)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 3; Car No. 3; 20 Fuels; Road ON Mean = 92.130

							Coefficients*	nts*		
Car Code	Egn.	Std. Dev.	R ²	Constant* bo	RON b1	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ²
0L 223	-	0.807	0.865	35.220 (0.0001)	0.602					
	2	0.961	0.808	$\frac{5.522}{(0.587)}$		1.010 (0.0001)				
	ო	0.555	0.939	13.950 (0.031)	0.378	0.495 (0.0003)				
	4	0.517	0.951	13.278 (0.028)	0.373	0.513	$\frac{-0.024}{(0.075)}$			
	រេះ	0.569	0.940	14.488 (0.033)	0.388	0.477 (0.0009)		0.013 (0.658)		
	9	0.531	0.951	13.852 (0.031)	0.380 (0.0001)	0.498 (0.0004)	$\frac{-0.024}{(0.087)}$	$\frac{0.011}{(0.704)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

Lab 7; Car No. 37; 17 Fuels (Except 2, 7, 17); Road ON Mean = 93.388 FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Coefficients*	Aromatics Ethanol (RON) ² (MON) ² $\begin{array}{cccc} & & & & & & & & \\ & & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & \\ & & \\ & & & \\ & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ $				0.007 (0.687)	$\frac{0.030}{(0.333)}$	0.006 0.029
	MON b2		0.788 (0.0002)	$\frac{0.146}{(0.222)}$			
	RON b ₁	0.564 (1.0001)		0.498 (0.0001)	0.566	0.569	0.571
	Constant*	40.040 (0.0001)	25.750 (0.077)	33.751 (0.0001)	39.738 (0.0001)	39.448 (0.0001)	39, 167
	R ²	0.915	0.625	0.924	0.916	0.920	0.921
	Std. Dev.	0.572	1.201	0.560	0.589	0.572	0.591
	Egn.	-	C)	ო	4a	Sа	9
	Car Code	OL 223					

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 7; Car No. 36; 17 Fuels (Except 2, 7, 17); Road ON Mean = 92.971

	(MON) ²						
	(RON) ² b ₆						
nts*	Ethanol b4					0.093 (0.028)	0.094 (0.031)
Coefficients*	Heavy Aromatics b ₃				-0.011 (0.604)		-0.012 (0.503)
	MON b2		0.911 (0.0001)	0.551	0.552	0.388	0.388
	RON b ₁	0.528		0.279 (0.0087)	0.275 (0.012)	0.370 (0.0009)	0.366 (0.0014)
	Constant* b ₀	43.028 (0.0001)	14.775 (0.189)	19.286 (0.045)	19.755 (0.047)	24.301 (0.0078)	24.869 (0.0087)
	R ²	0.748	0.780	0.868	0.870	0.910	0.914
	Std. Dev.	1.017	0.951	0.763	0.783	0.653	0.667
	Egn	-	8	ന	4	ហ	9
	Car Code	PC 137					

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 26; Car No. 19; 20 Fuels; Road ON Mean = 91.345

	(MON) ² b ₇								
	(RON) ² _b							-0.051 (0.0002)	-0.049
ents*	Ethanol b4					(0.052)	(0.051)		0.042 (0.047)
Coeffici	Heavy Aromatics Ethu b ₃ b ₂				-0.011 (0.513)		-0.010 (0.510)		
	MON b ₂		0.717 (0.0001)	$\frac{0.170}{(0.179)}$					
	RON b ₁	0.478		0.401	0.479	0.486	0.487	10.076 (0.0001)	9.653 (0.0001)
	Constant*	46.157 (0.0001)	29.862 (0.012)	38.859 (0.0001)	46.246 (0.0001)	45.164 (0.0001)	45.240 (0.0001)	-405.409 (0.0007)	-383.486 (0.0005)
	R ²	0.865	0.644	0.879	0.869	0.886	0.889	0.940	0.954
	Std. Dev.	0.639	1.039	0.623	0.649	0.605	0.615	0.437	0.397
	Eqn	~	8	က	48	ည	ба	20	23
	Car Code	PC 137							

Number in parentheses represents the probability that the number is not si_'ficant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

(Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 30; Car No. 25; 20 Fuels; Road ON Mean = 92.915

							Coefficients*	ints*		
Car Code	Egn.	Std. Dev.	R ²	Constant* bo	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
PC 137	-	1,257	0.756	31.089 (0.0014)	0.654					
	2	1.307	0.737	$\frac{-3.211}{(0.817)}$		1.121 (0.0001)				
	ო	1.058	0.837	5.335	0.384 (0.0048)	0.598				
	4	1.079	0.840	5.729 (0.625)	0.387 (0.0056)	0.587	0.016			
	ស	0.922	0.884	10.077	0.475	0.436		0.120 (0.023)		
	9	0.932	0.888	10.652 (0.309)	0.480	0.420 (0.047)	$\frac{0.019}{(0.431)}$	0.122 (0.023)		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 30; Car No. 26; 20 Fuels; Road ON Mean = 91.935

							Coefficients*	nts*		
Car Code	Egn.	Std. Dev.	R ²	Constant" bo	RON P ₁	HON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ²
PC 137	-	1.372	0.758	24.153 (0.016)	0.717					
	2	1.331	0.773	-15.939 (0.264)		1.258 (0.0001)				
	ю	1.081	0.858	-7.256 (0.536)	0.388 (0.0052)	0.729				
	4	1.044	0.876	-6.354 (0.578)	0.397 (0.0038)	0.701	0.039			
	ĸ	0,963	0.894	$\frac{-2.727}{(0.802)}$	0.476 (0.0007)	0.573		0.116 (0.033)		
	ø	0.896	0.914	-1:490 (0:882)	0.483	0.537 (0.011)	0.042 (0.081)	0.120		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 47; Car No. 32; 19 Fuels (Except 2); Road ON Mean = 92.616

							Coefficients*	nts*		
Car Code	Egn.	Std. Dev.	R2	Constant*	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b ₄	(RON) ² b ₆	(MON) ² b ₇
PL 217M	-	0.938	0.694	51.184 (0.0001)	0.437					
	8	0.626	0.864	22.114 (0.0046)		0.821				
	ო	0.549	0.901	24.575 (0.0009)	0.157	0.619 (0.0001)				
	4	0.516	0.918	24.828 (0.0006)	0.146 (0.028)	0.636 (0.0001)	-0.023 (0.099)			
	ស	0.567	0.901	24.434 (0.0016)	0.155 (0.039)	0.623		$\frac{-0.003}{(0.929)}$		
	9	0.534	0.918	24.315 (0.0012)	0.143	0.642 (0.0001)	-0.023 (0.111)	_0.004 (0.882)		
	æ	0.455	0.936	-305.502 (0.018)	7.189	0.572 (0.0001)			-0.037 (0.012)	
	01	0.396	0.955	-314.472 (0.0071)	7.368 (0.0038)	0.588 (0.0001)	-0.024 (0.030)		-0.038 (0.0043)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

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FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 50; Car No. 33; 20 Fuels; Road ON Mean = 89.725

	_	0.746	0.702 0.744	
(0.653)	38.298 (0.0001) 36.915 (0.0001) 36.380 (0.0001)		0.756	b 0.558 0.820 b 0.558 0.848

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR ≥ 0.05) are underlined.

TABLE F-8 (Continued)

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FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 41; Car No. 29; 18 Fuels (Except 2, 17); Road ON Mean = 94.489

							Coefficients*	nts*		
Car Code	Eqn.	Std. Dev.	R ²	Constant* b ₀	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² _{b6}	(MON) ²
T 218M		1.096	0.721	42.822 (0.0001)	0.546					
	8	1.430	0.525	$\frac{27.501}{(0.104)}$		0.781				
	က	1.093	0.740	33.149 (0.017)	0.447	$\frac{0.222}{(0.315)}$				
	4a	1.073	0.749	44.613 (0.0001)	0.533 (0.0001)		$\frac{-0.036}{(0.215)}$			
	Sа	1.014	0.776	40.992 (0.0001)	0.561 (0.0001)			$0.096 \\ (0.075)$		
	6a	0.990	0.801	42.669 (0.0001)	0.549 (0.000ī)		$\frac{-0.034}{(0.206)}$	$\frac{0.093}{(0.077)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-8 (Continued)

FULL-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 26, Car No. 18, 19 Fuels (Except 15); Road ON Mean = 92.574

	(MON) ²							
	(RON) ² b ₆							-0.631 (0.022)
ents*	Ethanol b ₄					0.096 (0.0036)	0.095	0.095 (0.0013)
Coefficie	Heavy Aromatics Etha				$\frac{-0.010}{(0.587)}$		-0.006 (0.662)	
	MON So		1.032 (0.0001)	0.656 (0.0003)	0.657 (0.0004)	0.540 (0.0003)	0.542 (0.0004)	0.525
	RON b ₁	0.604 (0.0001)		0.282	0.285 (0.0058)	0.343	0.345	6.242 (0.017)
	Constant* bo	35.620 (0.0001)	$\frac{4.110}{(0.651)}$	$\frac{9.750}{(0.209)}$	$(\frac{9.542}{0.230})$	13.481 (0.036)	13.223 (0.044)	-265.836 (0.028)
	R ²	0.790	0.850	0.910	0.911	0.950	0.950	996.0
	Std. Dev.	1.027	0.869	0.695	0.710	0.536	0.551	0.457
	Eqn.	-	8	က	4	ស	9	Ξ
	Car Code	T 222						

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>0.05) are underlined.

TABLE F-9

FULL-THROTTLE ROAD ON REGRESSION EQUATIONS

37 Cars; Individual Car Road ON Ratings (No Averaging); Road ON Mean = 91.904

	(RON) ²		~0.020 (0.0002)	-5.321
Coefficients*	Heavy Aromatics b ₃			-0.012 (0.015)
Coeffic	MON b2	0.465	0.430	0.437 (0.0001)
	RON b ₁	0.284 (0.0001)	4.004 (0.0001)	4.317 (0.0001)
	Constant*	25.954 (0.0001)	-144.749 (0.0013)	-165.815 (0.0004)
	R ²	0.638	0.645	0.648
	Std. Dev.	1.252	1.241	1.236
	Equation	ო	ω	10

* Number in parentheses represents the probability that the number is not significant.

TABLE F-10

PART-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; 12 Cars; Road ON Mean = 88.030

Palling and State of Control of C	(R+M)/2 b ₅								
	RxM b8								
	(MOH) ² b ₇								$\frac{-0.010}{(0.336)}$
ients*	(RON) ² b ₆							$\frac{-0.001}{(0.710)}$	
Coefficients*	Ethanol b ₄					$\frac{-0.007}{(0.347)}$	-0.008 (0.188)		
	Heavy Aromatics b ₃		٠		-0.00 <u>9</u> (0.0080)		-0.009 (0.0062)		
	MON b ₂		0.677	0.553	0.559	0.562 (0.0001)	0.570 (0.0001)	0.551	-1.179 (0.509)
	RON b ₁	0.341		0.091	0.089	0.086	0.083	$\frac{0.361}{(0.620)}$	0.093
	Constant*	55.794 (0.0001)	29.977 (0.0001)	32.008 (0.0001)	31.823 (0.0001)	31.740 (0.0001)	31.483 (0.0001)	15.591 (0.569)	106.807 (0.174)
	R ²	0.740	0.969	0.989	0.993	0.990	0.994	0.989	0.990
	Std. Dev.	0.684	0.238	0.144	0.119	0.145	0.115	0.148	0.144
	Egn.	-	~	က	4	ည	9	ထ	6

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

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PART-THROTTLE ROAD ON REGRESSION EQUATIONS

All-Car Averages; 12 Cars; Road ON Mean = 88.030

	(R+M)/2 b ₅							
	RxM b ₈							$\frac{0.025}{(0.522)}$
	(MON) ²			$\frac{0.011}{(0.199)}$	$\frac{0.010}{(0.331)}$		(0.011)	$\frac{-0.012}{(0.764)}$
ents*	(RON) ² b ₆	-0.003 (0.398)	$\frac{-0.002}{(0.674)}$			$\frac{-0.003}{(0.341)}$		$\frac{-0.011}{(0.414)}$
Coefficients*	ш		$\frac{-0.007}{(0.349)}$		$\frac{-0.007}{(0.341)}$	$\frac{-0.009}{(0.173)}$	-0.008 (0.170)	
	Heavy Aromatics b ₃	-0.009		-0.009 (0.0066)		-0.009 (0.0055)	-0.009 (0.0049)	
	MON b ₂	0.556 (0.0001)	0.561 (0.0001)	$\frac{-1.321}{(0.360)}$	$\frac{-1.193}{(0.505)}$	0.567	$\frac{-1.340}{(0.338)}$	$\frac{0.152}{(0.963)}$
	RON b ₁	$\frac{0.595}{(0.322)}$	0.393 (0.591)	0.091 (0.0001)	0.088	$\frac{0.638}{(0.276)}$	0.085	$\frac{-0.154}{(0.912)}$
	Constant*	11.056 (0.768)	$\frac{20.678}{(0.612)}$	$\frac{111.960}{(0.080)}$	$\frac{108.512}{(0.173)}$	$\frac{-20.749}{(0.837)}$	$\frac{114.193}{(0.070)}$	$\frac{73.437}{(0.538)}$
	R ²	0.993	0.990	0.994	0.994	0.994	0,995	0.990
	Std. Dev.	0.120	0.148 0.990	0.116 0.994	0.145 0.994	0.116	0.112 0.995	0.150 0.990
	Eqn.	10	Ξ	12	13	14	15	16

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

TABLE F-11

PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 29; Car No. 21; 20 Fuels; Road ON Mean = 89.215

· Carlotte in the carlotte in	(MON) ²							0.068 (0.014)
	(RON) ² b ₆							
nts*	Ethanol b ₄					$0.020 \\ (0.342)$	(0.020)	
Coefficients*	Heavy Aromatics b ₃				-0.009 (0.415)		$\frac{-0.008}{(0.445)}$	
	MON b2		0.810 (0.0001)	0.542 (0.0001)	0.549 (0.0001)	0.514 (0.0001)	0.521 (0.0081)	-11.083 (0.019)
	RON b ₁	0.441		0.196 (0.0006)	0.194 (0.0007)	0.212 (0.0005)	0.209 (0.0008)	0.210 (0.0001)
	Constant* b ₀	47.525 (0.0001)	19.757 (0.0038)	24.210 (0.0001)	23.948 (0.0001)	25.007 (0.0001)	24.823 (0.0001)	519.722 (0.011)
	R ²	0.790	0.883	0.943	0.945	0.946	0.948	0.961
	Std. Dev.	0.770	0.575	0.413	0.417	0.413	0.418	0.351
	Egn	-	2	က	4	.c	9	6
	Car Code	LIA 238						

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR.>0.05) are underlined.

TABLE F-11 (Continued)

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PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 29, Car No. 22; 20 Fuels; Road ON Mean = 87.620

	(MON) ²						
	(RON) ² b ₆						
nts*	Ethanol b4					$\frac{-0.015}{(0.552)}$	$\frac{-0.016}{(0.529)}$
Coefficients*	Heavy Aromatics b ₃				$\frac{-0.013}{(0.302)}$		$\frac{-0.013}{(0.302)}$
	MON b2		0.516 (0.0001)	0.500 (0.0001)	0.522 (0.0001)	0.521 (0.0001)	0.527 (0.0001)
	RON b1	0.238 (0.0003)		$\frac{0.012}{(0.834)}$			
	Constant*	65.121 (0.0001)	43.373 (0.0001)	43.611 (0.0001)	43.075 (0.0001)	43.013 (0.0001)	42.719 (0.0001)
	R ²	0.518	0.809	0.810	0.821	0.814	0.826
	Std. Dev.	0.778	0.489	0.502	0.487	0.498	0.496
	Eqn.	-	2	ო	4p	2 p	6 b
	Car Code	LIA 238					

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-11 (Continued)

PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 4; Car No. 5; 20 Fuels; Road ON Mean = 85.225

							Coefficients*	nts*		
Car Code	Egn.	Std. Dev.	R ²	Constant* b ₀	RON b ₁	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
NC5 225	-	0.558	0.769	56.865 (0.0001)	0.300					
	8	0.361	0.903	36.776 (0.0001)		0.565				
	ო	0.272	0.948	39.350 (0.0001)	0.117	0.406				
•	4	0.252	0.958	39.147 (0.0001)	0.134	0.414	$\frac{-0.012}{(0.073)}$			
	ഹ	0.280	0.948	39.363 (0.0001)	0.116 (0.0029)	0.407		$\frac{-0.001}{(0.963)}$		
	9	0.261	0.958	38.993 (0.0001)	0.113 (0.0024)	0.417	-0.012 (0.082)	-0.002 (0.885)		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-11 (Continued)

PART-THROTTLE ROAD ON REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 7, Car No. 35; 17 Fuels (Except 2, 7, 17); Road ON Mean = 83.847

							Coefficients	nts*		
Car Code	Eqn.	Std. Dev.	R ²	Cons tant*	RON b1	MON b2	Heavy Aromatics b ₃	Ethanol b4	(RON) ² b ₆	(MON) ² b ₇
		0.837	0.441	62.754 (0.0001)	0.223					
	7	0.466	0.826	39.470		0.517				
	ო	0.480	0.828	38.985 (0.0001)	-0.023 (0.692)	0.548 (0.0001)				
	4b	0.469	0.836	39.991 (0.0001)		0.513 (0.0001)	$\frac{-0.011}{(0.380)}$			
	2p	0.483	0.826	39.466 (0.0001)		0.517 (0.0001)		$\frac{0.001}{(0.955)}$		
	9 9	0.487	0.836	40.081		0.512 (0.0001)	$\frac{-0.012}{(0.395)}$	0.003		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR>G.O5) are underlined.

TABLE F-11 (Continued)

PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 7; Car No. 34; 17 Fuels (Except 2, 7, 17); Road ON Mean = 89.388

							Coefficients*	ints*		
Car Code	Eqn.	Std. Dev.	R2	Constant*	RON P	MON b ₂	Heavy Aromatics b ₃	Ethanol b4	(RON) ² be	(HON) ²
0 V250	~	0.969	0.637	52.877 (0.0001)	0.386 (0.0001)					
	2	0.694	0.814	26.042 (0.0045)		0.738				
	ო	099.0	0.843	28.106 (0.0023)	$\frac{0.127}{(0.131)}$	0.574 (0.0008)				
	4b	0.714	0.816	25.655 (0.0068)		0.741	(0.008)			
	5b	0.600	0.870	23.085 (0.0047)		0.776 (0.0001)		-0.077 (0.028)		
	6 b	0.614	0.874	22.482 (0.0073)		0.781	$\frac{0.011}{(0.550)}$	-0.078 (0.030)		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-11 (Continued)

PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 29; Car No. 23; 20 Fuels; Road ON Mean = 88.800

					:		Coefficients*	nts*		
- 00 00 10 10	5 1	Std.	22	Cons tant* bo	RON b	MON b ₂	Heavy Aromatics b ₃	Ethanol ba	$(RON)^2$ b_6	$(MON)^2$
						ļ	en e en			
0CA 133	-	0.741	0.711	56.374 (0.0001)	0.343					
	2	0.469	0.884	31.862 (0.0001)		0.664				
	ო	0.418	0.913	34.394 (0.0001)	0.112 (0.029)	0.511				
	4	0.405	0.923	34.078 (0.0001)	0.108	0.522	-0.015 (0.164)			
	S	0.416	0.919	33,456 (0.0001)	0.094	0.543		-0.023 (0.300)		
	9	0.399	0.930	32.978 (0.0001)	0.090 (0.078)	0.556 (0.0001)	$\frac{-0.015}{(0.145)}$	$\frac{-0.025}{(0.251)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

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PART-THROTILE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 29; Car No. 24; 20 Fuels; Road ON Mean = 90.750

							Coefficie	ents*		
Car Codo	£m:	Std. Dev.	R ²	Constant*	RON b ₁	MON P2	Heavy Aromatics Ethan b ₃ b ₄	Ethanol b ₄	(RON) ² b ₆	(MON) ²
0CA 133	-	0.728	0,825	46.602 (0.0001)	0.467					
	8	0,602	0.880	18.892 (0.0072)		0.838 (0.0001)				
	ო	0.368	0.958	24.074 (0.0001)	0.230	0.524 (0.0001)				
	4	0.367	0.961	23.829 (0.0001)	0.228 (0.0001)	0.531 (0.0001)	-0.010 (0.307)			
	တ	0.369	0.960	23.340 (0.0001)	0.216 (0.0001)	0.549 (0.0001)		-0.019 (0.341)		
	ဖ	0.366	0.963	23.023 (0.0001)	0.213	0.558 (0.0001)	-0.010 (0.284)	-0.020 (0.313)		
	ဆ	0.289	0.976	-198.329 (0.0078)	4.975 (0.0025)	0.492 (0.0001)			-0.025 (0.0036)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-11 (Continued)

PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 4; Car No. 8; 20 Fuels; Road ON Mean = 85.290

							Coefficie	ints*		
Car Code	Eqn.	Std. Dev.	R2	Cons tant *	RON b ₁	MON Lb2	Heavy Aromatics Ethar b ₃ b ₄	Ethanol b4	(RON) ²	(MON) ²
OCA 242	-	1.027	0.490	57.213 (0.0001)	0.297					
	7	0.444	0.905	25.1 <i>7</i> 9 (0.0001)		0.701				
	က	0.443	0.910	23,989 (0.0001)	-0.050 (0.324)	0.770				
	4 <i>b</i>	0.440	0.912	24.967 (0.0001)		0.706 (0.0001)	$\frac{-0.013}{(0.265)}$			
	25	0.446	0,909	25.603 (0.0001)		0.695		(0.020)		
	q ₉	0.443	0.916	25.378 (0.0001)		0.700	-0.012 (0.281)	0.019 (0.39T)		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

TABLE F-11 (Continued)

PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 5; Car No. 11; 20 Fuels; Road ON Mean = 89.960

							Coefficia	ents*		
Car Code	Egn.	Std. Dev.	R ²	Constant*	RON b ₁	MON b2	Heavy Aromatics Ethar b ₃ b ₄	Ethanol b4	(RON) ² b _G	(MON) ² b ₇
0CA 242	-	0.705	0.729	57.629 (0.0001)	0.342					
	0	0.512	0.857	34.823 (0.0001)		0.643 (0.0001)				
٠	ო	0.411	0.900	37.770 (0.0001)	0.133 (0.016)	0.462 (0.0001)				
	4	0.454	0.900	37.727 (0.0001)	0.132 (0.019)	0.464 (0.0001)	-0.002 (0.845)			
	r.	0.449	0,902	37.164 (0.0001)	0.122 (0.036)	0.482		-0.015. (0.537)		
	Q	0.463	0.903	37.136 (0.0001)	0.121 (0.044)	0.484 (0.0001)	-0.003 (0.823)	-0.015		
	ω	0.392	0.926	$\frac{-137.372}{(0.073)}$	4.568 (0.028)	0.432 (0.0001)			-0.023 (0.032)	

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

TABLE F-11 (Continued)

PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 4; Car No. 6; 20 Fuels; Road ON Mean = 87.850

							Coefficients*	nts*		
Car Code	Eqn.	Std. Dev.	R ²	Constant* bo	RON b ₁	. MON	Heavy Aromatics b ₃	Ethanol b ₄	(RON) ² b ₆	(MON) ²
0I V258	L-m	0.574	0.809	54.962 (0.0001)	0.348					
	2	0.422	0.897	33.237 (0.0001)		· 0.637 (0.0001)		•		
	ო	0.268	0.961	36.651 (0.0001)	0.158	0.423				
	4	0.254	0.967	36.517 (0.0001)	0.155	0.430	$\frac{-0.011}{(0.101)}$			
	ស	0.273	0.962	37.063 (0.0001)	0.165	0.410		$\frac{0.009}{(0.526)}$		
	y	0.259	0.968	36.857 (0.0001)	0.161 (0.0001)	0.419 (0.0001)	$\frac{-0.011}{(0.116)}$	$\frac{0.008}{(0.561)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR >0.05) are underlined.

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TABLE F-11 (Continued)

PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 7; Car No. 37; 17 Fuels (Except 2, 7, 17); Road ON Mean = 90.276

							Coefficients*	nts*		
	1	Std.	7	Constant* bs	RON b,	MON b ₂	Heavy Aromatics b ₃	Ethanol b _A	(RON) ² b ₆	(MON) ² b ₇
Car Code	Egn.	Dev.	χ		-	ļ)	
0L 223	-	066.0	0.657	51.306 (0.0001)	0.412 (0.0001)					
	8	0.555	0.892	20.492 (0.0051)		0.813 (0.0001)				
	ო	0.520	0.912	22.276 (0.0022)	$\frac{0.110}{(0.101)}$	0.671				
	4p	0.557	0.899	21.232 (0.0047)		0.807	$\frac{-0.014}{(0.359)}$			
	2p	0.570	0.894	21.037 (0.0061)		0.806 (0.0001)		(0.014)		
	Q9	0.572	0.901	21.872 (0.0057)		0.799	$\frac{-0.015}{(0.358)}$	$\frac{0.016}{(0.608)}$		

Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR.20.05) are underlined.

TABLE F-11 (Continued)

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PART-THROTTLE ROAD ON MULTIPLE REGRESSION EQUATIONS - INDIVIDUAL CARS

Lab 7; Car No. 36; 17 Fuels (Except 2, 7, 17); Road ON Mean = 88.406

							Coefficie	nts*		
Car Code	Eqn.	Std.	R ²	Constant* b ₀	RON b ₁	MON b2	Heavy Aromatics Ethar b ₃ b ₄	Ethanol b4	(RON) ² b ₆	(MON) ²
	_	0.692	0.724	56.530 (0.0001)	0.337					
	2	0.283	0.954	32.184 (0.0001)		0.655				
	ო	0.189	0.981	33.789 (0.0001)	0.101	0.525 (0.0001)				
	4	0.178	0.984	34.116 (0.0001)	0.098	0.526 (0.0001)	-0.008 (0.120)			
	ഹ	0.179	0.984	32.889 (0.0001)	0.084 (0.0035)	0.555 (0.0001)		$\frac{-0.017}{(0.124)}$		
	9	0.166	0.987	33.203 (0.0001)	0.082 (0.0030)	0.555	-0.008 (0.108)	$\frac{-0.016}{(0.111)}$		

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Number in parentheses represents the probability that the number is not significant. Constant and coefficients not significant at the 95% confidence level (PR > 0.05) are underlined.

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APPENDIX G

ANALYSIS OF VARIANCE RESULTS

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ANALYSIS OF VARIANCE RESULTS

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Full-Throttle Road ON Ratings

Table G-4 All-Car Averages

Part-Throttle Road ON Ratings

TABLE G-1

ANALYSIS OF VARIANCE - ALL-CAR AND SUBGROUP AVERAGES

FULL-THROTTLE ROAD ON RATINGS

Significance Probability*	0.0001 0.0001 0.0001	0.0001 0.0001 0.0001	6.0001 0.0001 0.0001	0.0001 0.0001 0.0001
4	99.5 557.0 2.3	82.3 514.2 2.2	86.1 529.6 2.3	50.4 380.1 2.2
Percent of Variation	19.60 65.19 6.94 8.27	17.00 67.45 6.80 8.75	17.30 67.32 6.88 8.50	11.62 72.94 5.79 9.65
Std. Dev. of Effect	0.946 1.724 0.563 0.614	0.867 1.726 0.548 0.622	0.868 1.712 0.547 0.609	0.692 1.734 0.488 0.631
Variance Component	0.894 2.973 0.317 0.377	0.751 2.980 0.300 0.387	0.754 2.932 0.300 0.370	0.479 3.008 0.239 0.398
Mean Sum of Squares	37.525 210.059 0.862 0.377	37.809 198.822 0.871 0.387	31.886 196.131 0.839 0.370	20.044 151.253 0.875 0.398
Degrees of Freedom	35 19 643 698	33 19 608 661	33 19 608 661	24 19 456 500
Source	All Cars (Ex. E 215)-36 Cars Cars (Labs) Fuels Cars x Fuels Error	All Auto. Trans. (Ex. E 215) - 34 Cars Cars (Labs) Fuels Cars x Fuels Error	All U.S. Cars - 34 Cars Cars (Labs) Fuels Cars x Fuels Error	Cars Testing Ail Fuels (Ex. E 215) - 25 Cars Cars (Labs) Fuels Cars x Fuels Error

95% Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

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TABLE G-1 (Continued)

ANALYSIS OF VARIANCE - ALL-CAR AND SUBGROUP AVERAGES

FULL-THROTTLE ROAD ON RATINGS

Significance F Probability*	5.4 0.025 16.6 0.0001 0.6 0.870	0.1 0.816 17.9 0.0001 0.8 0.676	261.3 0.0001 34.0 0.0001 2.6 0.0050
Percent of Variation	3.58 77.61 0.00 18.81	0.00 81.02 0.00 18.98	40.21 48.64 5.04 6.20
Std. Dev. of Effect	0.353 1.640 0.807	1.872	1.182 1.301 0.419
Variance Component	0.124 2.691 -0.139 0.652	-0.016 3.504 -0.075 0.821	1.397 1.694 0.175
Mean Sum of Squares	3.539 10.790 0.390 0.652	0.045 14.685 0.670 0.821	56.448 7.342 0.567
Degrees of Freedom	- 6 8 9 9 9 9 9 9	1 19 40	L 0 0 C
Source	HIK 238 - 2 Cars Cars (Labs) Fuels Cars x Fuels Error	LIA 238 - 2 Cars Cars Fuels Cars x Fuels Error	NC5 225/HC5 225 - 2 Cars Cars (Labs) Fuels Cars x Fuels

^{95%} Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% -0.0001

TABLE G-1 (Continued)

ANALYSIS OF VARIANCE - ALL-CAR AND SUBGROUP AVERAGES

FULL-THROTTLE ROAD ON RATINGS

Significance Probability*	0.0001 0.0001 0.599	0.0001 0.0001 0.630	0.044 0.0001 0.0008
ഥ	18.4 73.5 0.9	355.4 49.1 0.9	9.00 9.00 9.00 9.00
Percent of Variation	2.22 92.67 0.00 5.11	49.78 44.80 0.29 5.13	0.11 91.44 4.48 3.97
Std. Dev. of Effect	0.255 1.646 0.380	1.728 1.639 0.132 0.554	0.057 1.675 0.371 0.349
Variance Component	0.065 2.709 -0.008 0.149	2.985 2.686 0.017 0.307	0.003 2.806 0.137 0.122
Mean Sum of Squares	2.738 10.968 0.132 0.149	109.256 15.083 0.276 0.307	0.528 11.620 0.397 0.122
Degrees of Freedom	19 19 40	2 19 35 57	1 19 40
Source	NIK 238 - 2 Cars Cars (Labs) Fuels Cars x Fuels Errors	0 V250/M V250 - 3 Cars Cars (Labs) Fuels Cars x Fuels Error	OCA 133 - 2 Cars Cars Fuels Cars x Fuels Error

95% Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

TABLE G-1 (Continued)

ANALYSIS OF VARIANCE - ALL-CAR AND SUBGROUP AVERAGES

FULL-THROTTLE ROAD ON RATINGS

Significance Probability*	0.0001 0.0001 0.113	0.0001 0.0001 0.018	0.0001 0.0001 0.121
ı	41.8 148.9 1.6	60.2 36.7 2.3	17.0 31.7 1.3
Percent of Variation	2.57 94.14 0.73 2.56	14.90 71.85 5.47 7.78	9.20 69.53 3.51 17.76
Std. Dev. of Effect	0.338 2.046 0.180 0.337	0.867 1.905 0.525 0.627	0.757 2.080 0.468 1.051
Variance Component	0.114 4.185 0.033 0.114	0.752 3.629 0.276 0.393	0.573 4.327 0.219 1.105
Mean Sum of Squares	4.753 16.919 0.179 0.114	23.647 14.428 0.903 0.393	18.817 34.992 1.475
Degrees of Freedom	19 19 40	1 19 16 37	3 54 77
Source	OCA 242 - 2 Cars Cars (Labs) Fuels Cars x Fuels Error	OL 223 - 2 Cars Cars (Labs) Fuels Cars x Fuels Error	PC 137 - 4 Cars Cars (Labs) Fuels Cars x Fuels Error

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^{95%} Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

TABLE G-2

ANALYSIS OF VARIANCE - INDIVIDUAL LABORATORIES

Source	Degrees of Freedom	Mean Sum of Squares	Variance Component	Std. Dev. of Effect	Percent of Variation	ᄕ	Significance Probability*
Laboratory 3 - 4 Cars Cars Fuels Cars x Fuels Error	3 19 57 80	0.859 24.198 0.540 0.424	0.008 2.957 0.058 0.424	0.089 1.720 0.240 0.651	0.23 85.79 1.67 12.31	2.0 57.0 1.3	0.116 0.0001 0.160
Laboratory 4 - 4 Cars Cars Fuels Cars x Fuels Error	3 19 57 80	23.000 18.381 0.682 0.113	0.558 2.212 0.284 0.113	0.747 1.487 0.533 0.337	17.61 69.84 8.97 3.58	202.8 162.0 6.0	0.0001 0.0001 0.0001
Laboratory 5 - 3 Cars Cars Fuels Cars x Fuels Error	19 38 60	7.448 29.400 0.969 0.110	0.162 4.738 0.430 0.110	0.402 2.177 0.655 0.332	2.98 87.09 7.90 2.03	67.6 266.7 8.8	0.0001 0.0001 0.0001
Laboratory 7 - 4 Cars Cars Fuels Cars x Fuels Error	3 16 48 68	47.772 22.212 0.778 0.319	1.382 2.679 0.230 0.319	1.176 1.637 0.479 0.565	29.98 58.12 4.98 6.92	149.7 69.6 2.4	0.0001 0.0001 0.0004

* 95% Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

TABLE G-2 (Continued)

ANALYSIS OF VARIANCE - INDIVIDUAL LABORATORIES

Source	Degrees of Freedom	Mean Sum of Squares	Variance Component	Std. Dev. of Effect	Percent of Variation	4	Significance Probability*
Laboratory 8 - 5 Cars Cars Fuels Cars x Fuels Error	4 19 76 100	9.545 20.197 0.208 0.105	0.233 1.999 0.051 0.105	0.483 1.414 0.226 0.325	9.77 83.68 2.14 4.41	90.5 191.5 2.0	0.0001 0.0001 0.0008
Laboratory 26 - 4 Cars Cars Fuels Cars x Fuels Error	3 19 56 79	43.275 25.815 0.776 0.625	1.075 3.160 0.106 0.625	1.637 1.778 0.326 0.790	21.65 63.63 2.14 12.58	69.3 1.2	0.0001 0.0001 0.186
Laboratory 29 - 4 Cars Cars Fuels Cars x Fuels Error	3 19 57 80	10.634 4.359 0.464 0.471	0.254 3.189 -0.004 0.471	0.504 1.786 0.687	6.49 81.47 0.00 12.04	22.6 55.1 1.0	0.0001 0.0001 0.520
Laboratory 30 - 2 Cars Cars Fuels Cars x Fuels Error	1 19 40	19.701 25.981 0.996 1.530	0.468 6.250 -0.292 1.580	0.684 2.500 1.257	5.63 75.33 0.00 19.04	12.5 0.6 0.6	0.0011 0.0001 0.859

^{95%} Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 59.99% - 0.0001

(Continued)

ANALYSIS OF VARIANCE - INDIVIDUAL LABORATORIES

Source	Degrees of Freedom	Mean Sum of Squares	Variance Component	Std. Dev. of Effect	Percent of Variation	ir.	Significance Probability*
Laboratory 35 - 2 Cars Cars Fuels Cars x Fuels Error	1 18 38	14.329 10.679 0.188 0.529	0.372 2.623 -0.171 0.529	0.610 1.620 0.727	10.56 74.42 0.00 15.02	27.1 20.2 0.4	0.0001 0.0001 0.989
Laboratory 41 - 3 Cars Cars Fuels Cars x Fuels Error	34 34 54	152.762 20.695 1.902 0.190	4.191 3.132 0.857 0.190	2.047 1.770 0.925 0.436	50.08 37.43 10.22 2.27	803.2 108.8 10.0	0.0001 0.0001 0.0001
Laboratory 47 - 1 Car Cars Fuels Cars x Fuels Error	0 8 0 6	5.487	2.725	1.651	98.68	151.1	0.0001
Laboratory 50 - 1 Car Cars Fuels Cars x Fuels Error	ဝဋီဝဝ	1.428					

^{* 95%} Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

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TABLE G-3

ANALYSIS OF VARIANCE - INDIVIDUAL CARS

FULL-THROTTLE ROAD ON RATINGS

Source	Degrees of Freedom	Mean Sum of Squares	Variance Component	Std. Dev. of Effect	Percent of Variation	11.	Significance Probability*
Fuels Error	19	4.686 0.264	2.111	1.487	89.35 10.65	17.8	0.0001
HIA 238 - Lab 8 (13) Fuels Error	19 20	2.834 0.105	1.365 0.105	1.168	92.87 7.13	27.1	0.0001
HIK 238 - Lab 3 (4) Fuels Error	19	6.307	2.904	1.704	85.32 14.68	12.6	0.0001
HIK 238 - Lab 35 (27) Fuels Error	8 8	4.911 0.842	2.094 0.842	1.447	71.32 28.68	დ. დ	0.0003
HLV 225 - Lab 41 (30) Fuels Error	17	11.120 0.082	5.519 0.082	2.349	98.53 1.47	134.8	0.0001
IIF 243 - Lab 41 (31) Fuels Error	17	5.155	2.526 0.102	1.589	96.11 3.89	50.4	0.0001

95% Probability - 0.05; 99% - 0.01; 99.9% · 0.001; 99.99% - 0.0001

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(Continued)

ANALYSIS OF VARIANCE - INDIVIDUAL CARS

Source	Degrees of Freedom	Mean Sum of Squares	Variance Component	Std. Dev. of Effect	Percent of Variation	14	Significance Probability*
KI 137 - Lab 5 (10) Fuels Error	19 20	16.768 0.054	8.357 0.054	2.891 0.233	99.35 0.65	307.7	0.0001
LIA 238 - Lab 29 (21) Fuels Error	19 20	9.942	4.282	2.069	75.64 24.36	7.2	0.0001
LIA 238 - Lab 29 (22) Fuels Error	19 20	5.412 0.263	2.575 0.263	1.605 0.513	90.74 9.26	20.6	0.0001
M V250 - Lab 8 (16) Fuels Error	19 20	4.758 0.156	2.301 0.156	1.517	93.65 6.35	30.5	0.0001
NC5 225 - Lab 4 (5) Fuels Error	19 20	3.223 0.168	1.527 0.168	1.236 0.410	90.06	19.1	0.0001
NC7 228 - Lab 26 (20) Fuels Error	19 20	6.629 0.895	2.867 0.895	1.693 0.946	76.20 23.80	7.4	0.0001

95% Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

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TABLE G-3 (Continued)

ANALYSIS OF VARIANCE - INDIVIDUAL CARS

Source	Degrees of Freedom	Mean Sum of Squares	Variance Component	Std. De. of Effect	Percent of Variation	ш	Significance Probability*
NFH 450 - Lab 8 (15) Fuels Error	19 20	3.923 0.113	1.905	1.380	94.39 5.61	34.6	0.0001
NH 450 - Lab 8 (14) Fuels Error	19 20	5.291 0.104	2.594 0.104	1.610 0.322	96.14 3.86	50.9	0.0001
NIG 230 - Lab 35 (28) Fuels Error	18 19	5.695 0.246	2.724 0.246	1.651 6.496	91.72 8.28	21.3	0.0001
NIJ 244 - Lab 8 (12) Fuels Error	19 20	4,222 0.049	2.087 0.049	1.444	97.69	85.7	0.0001
NIK 238 - Lab 4 (7) Fuels Error	19 20	4.498 0.179	2.384 0.179	1.544 0.423	93.01 6.99	27.6	0.0001
NIK 238 - Lab 5 (9) Fuels Error	1 <u>9</u> 20	6.152 0.119	3.016 0.119	1.737	96.20 3.80	51.6	0.0001

^{95%} Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

TABLE G-3 (Continued)

ANALYSIS OF VARIANCE - INDIVIDUAL CARS

FULL-THROTTLE ROAD ON RATINGS

Source	Degrees of Freedom	Mean Sum of Squares	Variance Component	Std. Dev. of Effect	Percent o° Variation	ĹĹ	Significance Probability*
NL9 216 - Lab 7 (35) Fuels Error	16 17	3.697 0.242	1.728	1.314 0.492	87.72 12.28	15.3	0.0001
0 V250 - Lab 3 (1) Fuels Error	19 20	5.724 0.533	2.596 0.533	1.611 0.730	82.96 17.04	10.7	0.0001
0 V253 - Lab 7 (34) Fuels Error	16 17	6.083 0.220	2.932 0.220	1.712	93.03 6.97	27.7	0.0001
OCA 133 - Lab 29 (23) Fuels Error	15 20	6.218 0.117	3.050 0.117	1.746 0.342	96.30 3.70	53.0	0.0001
OCA 133 - Lab 29 (24) Fuels Evror	19 20	5.799 0.126	2.836 0.126	1.684 0.356	95.73 4.27	45.8	0.0001
OCA 223 - Lab 26 (17) Fuels Error	19 20	6.878 0.270	3.304 0.270	1.818 0.519	92.46 7.54	25.5	0.0001

95% Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

TABLE G-3 (Continued)

ANALYSIS OF VARIANCE - INDIVIDUAL CARS

Source	Degrees of Freedom	Mean Sum of Squares	Variance Component	Std. Dev. of Effect	Percent of Variation	ıL	Significance Probability*
OCA 242 - Lab 4 (8) Fuels irror	19 20	8.679 0.070	4.304	2.075 0.265	98.39 1.61	123.6	0.0001
OCA 242 - Lab 5 (11) Fuels Error	19 20	8.419 0.157	4.131 0.157	2.032 0.396	96.34 3.66	53.6	0.0001
OI V258 - Lab 4 (6) Fuels Error	19 20	3.576 0.036	, .770 0.036	1.330	98.02 1.98	100.0	0.0001
OL 223 - Lab 3 (3) Fuels Error	19 20	9.100 0.402	4.349 0.402	2.086 0.634	91.55 8.45	22.7	0.0001
OL 223 - Lab 7 (37) Fuels Error	16 17	7.137 0.383	3.377 0.383	1.838 0.619	89.82 10.18	18.6	0.0001
PC 137 - Lab 7 (36) Fuels Error	16	7.629 0.432	3.598 0.432	1.897	89.28 10.72	17.7	0.0001

^{• 95%} Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

TABLE G-3 (Continued)

ANALYSIS OF VARIANCE - INDIVIDUAL CARS

FULL-THROTTLE ROAD ON RATINGS

Significance Probability*	0.0001	0.0001	0.0001	0.0001		0.0001	0.0001
4	7.9	1.1	7.2	151.1		21.3	15.5
Percent of Variation	77.60 22.40	83.46 16.54	75.49 24.51	98.68 1.32		91.04 8.96	87,90 12,10
Std. Dev. of Effect	1.588 0.853	2.368	2.512 1.431	1.651 0.191		1.979 0.621	2.097 0.778
Variance Component	2.522 0.728	5.606	6.311 2.048	2.725 0.036		3.918 0.386	4.398
Mean Sum of Squares	5.772 0.728	12.324	14.670 2.048	5.487 0.036	1.428	8.223 0.386	9.402 0.606
Degrees of Freedom	19 20	19 20	19 20	18 19	91 0	17 18	18 19
Source	PC 137 ~ Lab 26 (19) Fuels Error	PC 137 - Lab 30 (25) Fuels Error	PC 137 - Lab 30 (26) Fuels Error	PL 217M - Lab 47 (32) Fuels Error	E 215 - Lab 50 (33) Fuels Error	T 218M - Lab 41 (29) Fuels Error	T 222 - Lab 26 (18) Fuels Error

^{* 95%} Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

TABLE G-4

ANALYSIS OF VARIANCE - ALL-CAR AVERAGES

PART-THROTTLE ROAD ON RATINGS

Significance Probability*		0.0001 0.0001 1.000
14		205.1 44.0 0.5
Percent of Variation		64.65 23.10 0.00 12.25
Std. Dev. of Effect		2.153 1.287 0.937
Variance Component		4.636 1.657 -0.099 0.879
Mean Sum of Squares		130.158 38.626 0.492 0.879
Degrees of Freedom		11 19 197 228
Source	All Cars - 12 Cars	Cars Fuels Cars x Fuels Error

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^{* 95%} Probability - 0.05; 99% - 0.01; 99.9% - 0.001; 99.99% - 0.0001

A P P E N D I X H

DETAILED TEST RESULTS

INDEX OF APPENDIX H

Glossary of Terms

Tabulation by Car Model

GLOSSARY OF TERMS

LAB NO Rating Participant - CRC Confidential Code

CAR CODE Car Identification - CRC Confidential Code

EM CT Emission Certification: F=Federal, C=California

TRANS Transmission Type: A=Automatic, M=Manual

C.R. Compression Ratio

AIR CND Air Conditioned: Y=Yes, N=No

ODOM MILES Odometer Miles on Car

STD SPK Basic Spark Advance Setting

TEST LOC D = Rating Performed on Chassis Dynamometer

RUN NO Number of Test Replicates

G Gear: D=Drive, P=Passing, 4=Fourth

DATE Month, Day, and Year Tested

AMB TMP Dry Bulb Temperature on Test Date, °F

BARO Barometric Pressure on Test, "Hg

HUM Relative Humidity, %

FUEL NO Fuels Described in Appendix B

SPK ADV Engine Spark Advance, Degrees

RPM Engine Speed, RPM

MUON Road Octane Number by Modified Uniontown Technique

Described in Appendix D

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